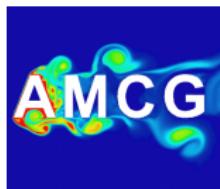


Exponential integrators and two-scale approaches for unsaturated water flow in heterogeneous soils

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NORMS Meeting, 26 November 2014

Overview of Presentation

- ▶ Modelling of unsaturated water flow
- ▶ Time integration methods for unsaturated water flow: Exponential integrators
- ▶ Two-scale numerical modelling of unsaturated water flow in soils exhibiting small-scale heterogeneities

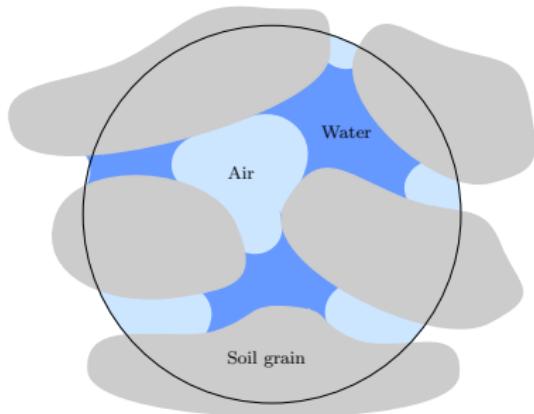
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Unsaturated water flow

- ▶ Immiscible two-phase (air and water) flow
- ▶ Darcy's Law:

$$\mathbf{q}_\alpha = -\frac{k_{r,\alpha}}{\mu_\alpha} K (\nabla p_\alpha - \rho_\alpha \mathbf{g})$$



- ▶ Capillary pressure $p_c = p_a - p_w$
- ▶ Mass conservation for each phase (assuming incompressibility)

$$\sum_{\alpha \in \{a,w\}} \mathbf{q}_\alpha = \mathbf{0}, \quad \frac{\partial (\phi S_\alpha)}{\partial t} + \nabla \cdot \mathbf{q}_\alpha = 0$$

- ▶ Sum of saturations $S_w + S_a = 1$

Richards' equation

- ▶ Assumptions:
 - (a) air phase is at constant and atmospheric pressure
 - (b) gravity acts in the negative y direction (2D)
- ▶ Single equation for the water phase:

$$\frac{\partial \theta(h)}{\partial t} + \nabla \cdot (-K(h)\nabla(h + x_2)) = 0$$

where $h = p_c/(\rho_w g)$ is the capillary pressure head, $\theta = \phi S_w$ is the moisture content and K is the hydraulic conductivity.

- ▶ Closure relationships [van Genuchten (1980)]:

$$\theta(h) = \theta_r + (\theta_s - \theta_r)S_e(h)$$

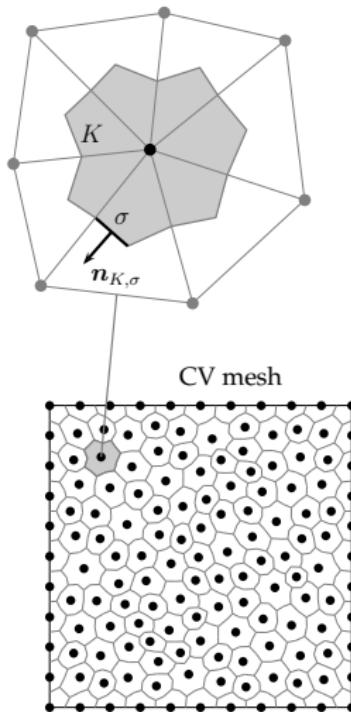
$$K(h) = K_{\text{sat}} \sqrt{S_e} \left(1 - \left(1 - S_e^{1/m} \right)^m \right)^2$$

$$S_e(h) = (1 + (-\alpha h)^n)^{-m}$$

Overview of Presentation

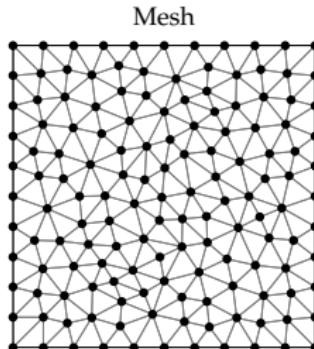
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Control Volume Method



Spatial discretisation:

$$\frac{d}{dt} \int_K \theta dV + \sum_{\sigma \subset \partial K} \int_{\sigma} -K(h) \nabla (h + x_2) \cdot \mathbf{n}_{K,\sigma} dS = 0$$



Time integration methods

- ▶ Spatial discretisation can be expressed in the form

$$\frac{d\mathbf{u}}{dt} = \mathbf{g}(\mathbf{u}), \quad \mathbf{u}(0) = \mathbf{u}_0 \in \mathbb{R}^N,$$

where $\mathbf{u} = (h_1, \dots, h_N)^T$ and N is the number of nodes.

- ▶ Classical explicit and implicit methods

$$\mathbf{u}_{n+1} - \mathbf{u}_n = \int_{t_n}^{t_{n+1}} \mathbf{g}(\mathbf{u}) dt$$

$$\mathbf{u}_{n+1} - \mathbf{u}_n = \tau_n \mathbf{g}(\mathbf{u}_n) \qquad \qquad \textit{Forward Euler method}$$

$$\mathbf{u}_{n+1} - \mathbf{u}_n = \tau_n \mathbf{g}(\mathbf{u}_{n+1}) \qquad \qquad \textit{Backward Euler method}$$

$$\mathbf{u}_{n+1} - \mathbf{u}_n = \tau_n [(1 - \theta) \mathbf{g}(\mathbf{u}_n) + \theta \mathbf{g}(\mathbf{u}_{n+1})] \quad \textit{Theta method}$$

where $\theta = 1/2$ gives the classical Crank-Nicolson method.

- ▶ Fluidity/IC-FERST uses the Theta method.

Exponential integrators

An *exponential integrator* is any time integration method that involves the exponential of the Jacobian matrix [Minchev and Wright (2005)]

Prototype method (Exponential Euler): At each time step, solve the linearised problem:

$$\frac{d\mathbf{u}}{dt} = \mathbf{g}(\mathbf{u}) \quad \xrightarrow{\text{Linearise}} \quad \frac{d\mathbf{u}}{dt} = \mathbf{g}_n + \mathbf{J}_n(\mathbf{u} - \mathbf{u}_n)$$

where $\mathbf{g}_n = \mathbf{g}(\mathbf{u}_n)$ and $\mathbf{J}_n = \mathbf{J}(\mathbf{u}_n)$, exactly over a single time step:

$$\mathbf{u}_{n+1} = \mathbf{u}_n + \tau_n \varphi(\tau_n \mathbf{J}_n) \mathbf{g}_n$$

where $\varphi(\mathbf{A}) = \mathbf{A}^{-1}(e^{\mathbf{A}} - \mathbf{I})$.

- ▶ Explicit
- ▶ Second order [Hochbruck et al. (1998)]
- ▶ Exact for linear problems \Rightarrow A-stable in the linear stability sense

Krylov subspace methods for matrix functions

- ▶ Extract an approximation from a small m dimensional Krylov subspace

$$\mathcal{K}_m(\mathbf{J}_n, \mathbf{g}_n) = \text{span} \{ \mathbf{g}_n, \mathbf{J}_n \mathbf{g}_n, \dots, \mathbf{J}_n^{m-1} \mathbf{g}_n \} \subset \mathbb{R}^N$$

- ▶ Construct an orthonormal basis for the subspace using Arnoldi's method

$$\mathbf{J}_n \mathbf{V}_m = \mathbf{V}_m \mathbf{H}_m + \beta_m \mathbf{v}_{m+1} \mathbf{e}_m^T$$

where the columns of $\mathbf{V}_m = [\mathbf{v}_1, \dots, \mathbf{v}_m]$ form an orthonormal basis for \mathcal{K}_m .

- ▶ Arnoldi's method requires only matrix-vector products with \mathbf{J}_n

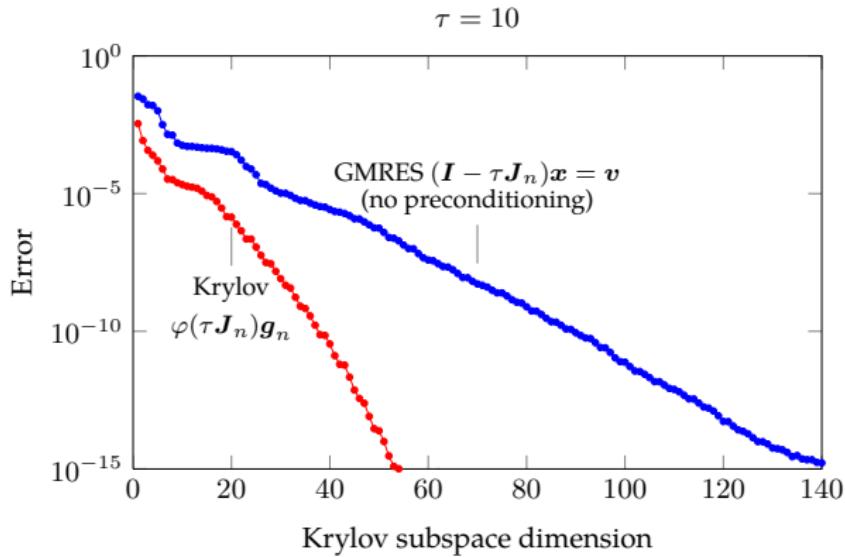
$$\mathbf{J}_n \mathbf{v} \approx [\mathbf{g}(\mathbf{u}_n + \varepsilon \mathbf{v}) - \mathbf{g}(\mathbf{u}_n)]/\varepsilon$$

- ▶ Standard Krylov subspace approximation [Hochbruck et al. (1998)]

$$\varphi(\tau_n \mathbf{J}_n) \mathbf{g}_n \approx \mathbf{V}_m [\|\mathbf{g}_n\|_2 \varphi(\tau_n \mathbf{H}_m) \mathbf{e}_1]$$

- ▶ Very accurate approximations can be obtained for $m \ll N$ so the matrix $\varphi(\tau \mathbf{H}_m)$ can be computed cheaply (e.g., using Padé approximation).

One attraction of exponential integrators



Higher order exponential integrators

- ▶ Write the ODE system in the form

$$\frac{d\mathbf{u}}{dt} = \mathbf{g}_n + \mathbf{J}_n(\mathbf{u} - \mathbf{u}_n) + \mathbf{r}(\mathbf{u}),$$

where $\mathbf{r}(\mathbf{u}) = \mathbf{g}(\mathbf{u}) - \mathbf{g}_n - \mathbf{J}_n(\mathbf{u} - \mathbf{u}_n)$.

- ▶ Using the integrating factor $e^{-t\mathbf{J}_n}$:

$$\frac{d}{dt} \left(e^{-t\mathbf{J}_n} \mathbf{u}(t) \right) = e^{-t\mathbf{J}_n} (\mathbf{g}_n - \mathbf{J}_n \mathbf{u}_n) + e^{-t\mathbf{J}_n} \mathbf{r}(\mathbf{u}).$$

the exact solution can be expressed as

$$\mathbf{u}(t_{n+1}) = \mathbf{u}_n + \tau_n \varphi_1(\tau_n \mathbf{J}_n) \mathbf{g}_n + \int_{t_n}^{t_{n+1}} e^{(t_{n+1}-t)\mathbf{J}_n} \mathbf{r}(\mathbf{u}) dt.$$

- ▶ This formula is the starting point for developing higher order methods [Tokman (2006), Hochbruck et al. (2009)].

Backward Differentiation Formula (BDF)

- ▶ Higher-order generalisations of the Backward Euler method
- ▶ Evaluate ODE system at $t = t_{n+1}$ to give

$$\frac{d\mathbf{u}}{dt}(t_{n+1}) = \mathbf{g}(\mathbf{u}_{n+1})$$

- ▶ For a BDF of order q : Interpolate the solution at $(t_{n+1-i}, \mathbf{u}_{n+1-i})$, $i = 0, \dots, q$ using a polynomial of degree q :

$$\mathbf{u}(t) \approx \sum_{i=0}^q \ell_i(t) \mathbf{u}_{n+1-i} \quad \ell_i(t) = \prod_{\substack{j=0 \\ j \neq i}}^q \frac{t - t_{n+1-j}}{t_{n+1-i} - t_{n+1-j}}$$

where $\ell_i(t)$ are the usual Lagrange interpolating polynomials.

- ▶ Differentiate interpolant and evaluate at $t = t_{n+1}$ to obtain

$$\frac{d\mathbf{u}}{dt}(t_{n+1}) \approx \sum_{i=0}^q \ell'_i(t) \mathbf{u}_{n+1-i}$$

Tested schemes

Exponential integrators

- ▶ Exponential Euler method (2nd order) [Carr et al. (2011)]
- ▶ Exponential Rosenbrock method (4th order) [Hochbruck et al. (2009)]
- ▶ At every time step, the error is estimated $\varepsilon_{n+1} \approx \mathbf{u}_{n+1} - \hat{\mathbf{u}}_{n+1}$ using an embedded method $\hat{\mathbf{u}}_{n+1}$ and the time step adjusted to satisfy user prescribed error tolerances. Stepsize accepted if $\|\varepsilon_{n+1}\|_{tol} \leq 1$ where

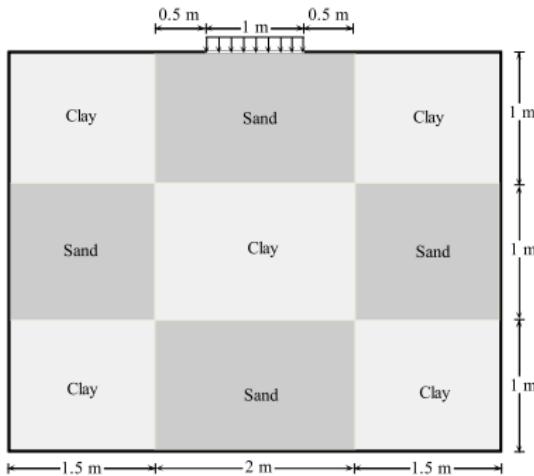
$$\|\mathbf{y}\|_{tol} = \|\mathbf{x}\|_2 / \sqrt{N}, \quad x_i = y_i / (tol_a + u_{n,i} tol_r)$$

Backward Differentiation Formulae (BDF)

- ▶ BDF Methods of order 2 and 4
- ▶ CVODE module of SUNDIALS [Hindmarsh et al. (2005)]
- ▶ Employs Newton iteration with an ILU preconditioned GMRES method.
- ▶ Periodically adjusts the order, with the goal of maximizing the stepsize
- ▶ Stepsize control

Test Case: Unsaturated water flow

- ▶ Test Case [Kirkland et al. (1992), McBride et al. (2006), Carr et al. (2011, 2013)]

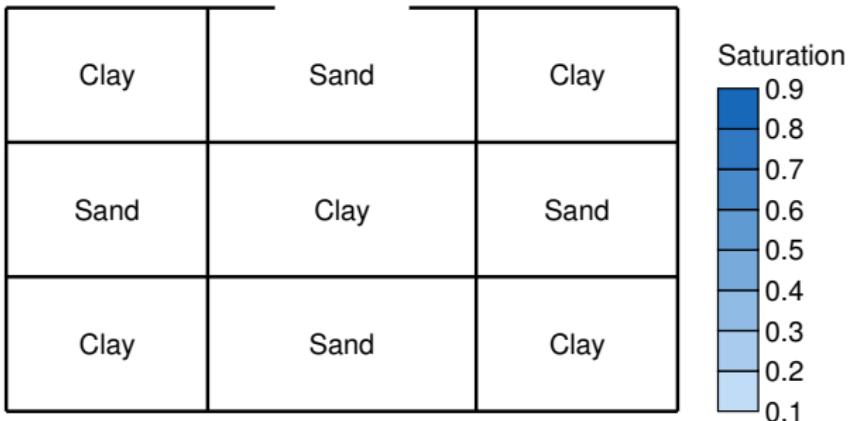


	Sand	Clay
K_{sat}	6.262e-5	1.516e-6
θ_r	0.0286	0.1060
θ_s	0.3658	0.4686
α	2.80	1.04
n	2.2390	1.3964

- ▶ Mesh: 132×132 grid, $N = 16641$.

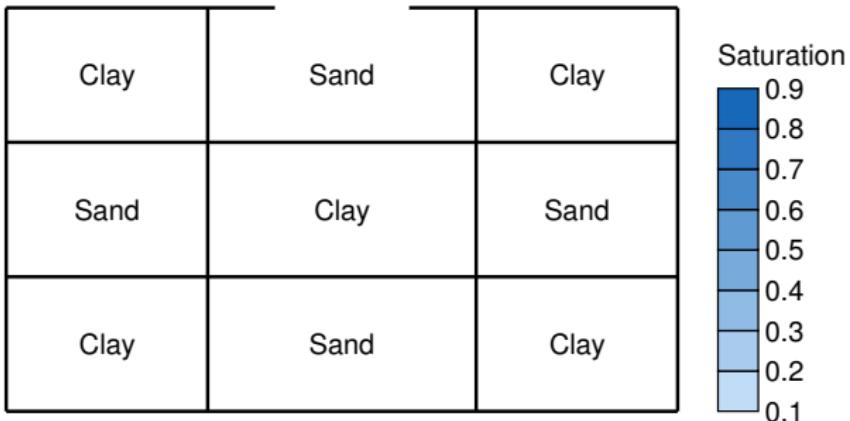
Test Problem: Water infiltration

$$q \cdot n = -5 \text{ cm/day}$$



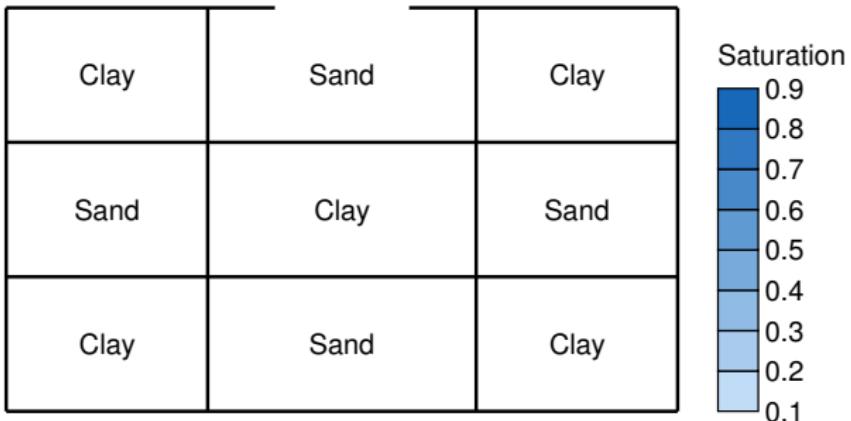
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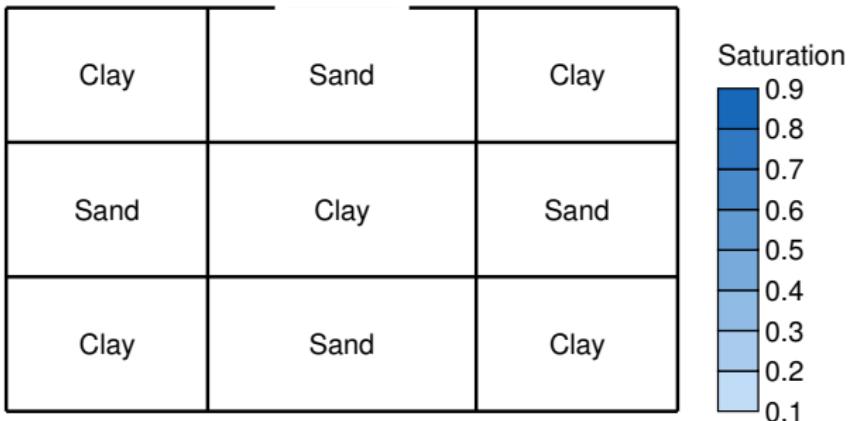
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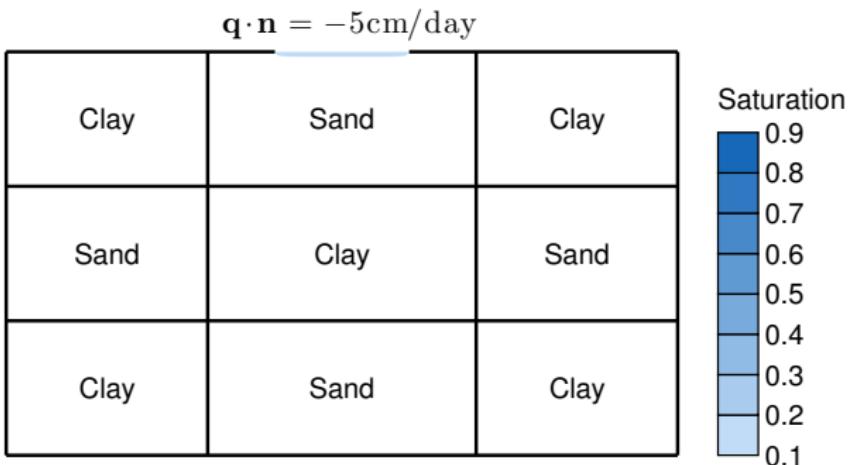


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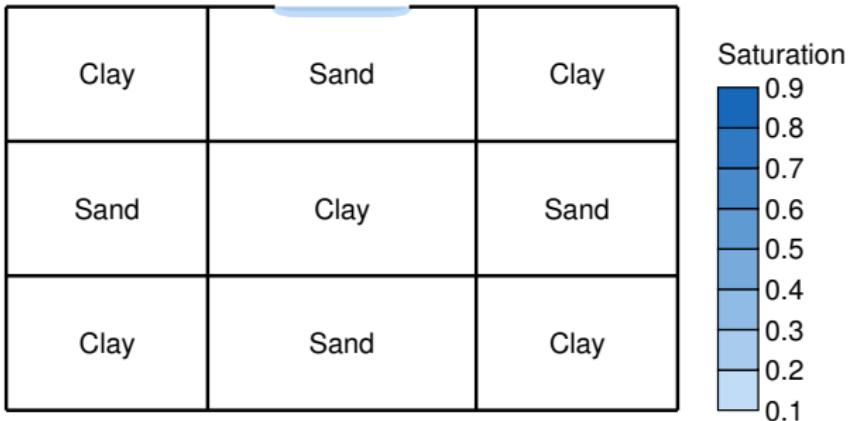


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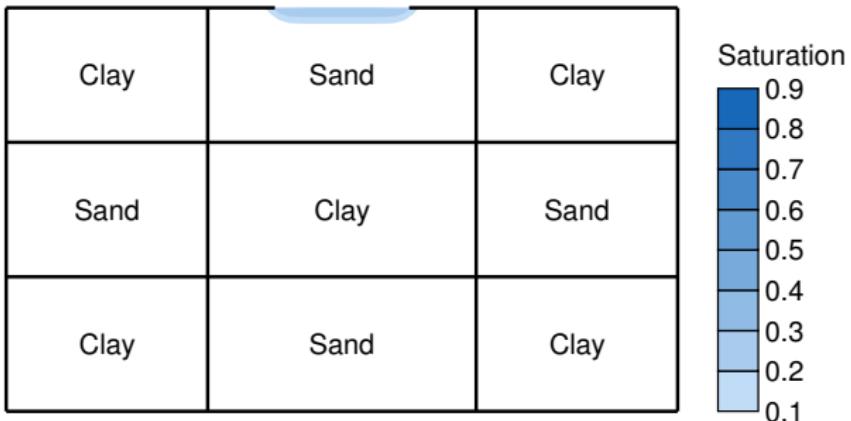
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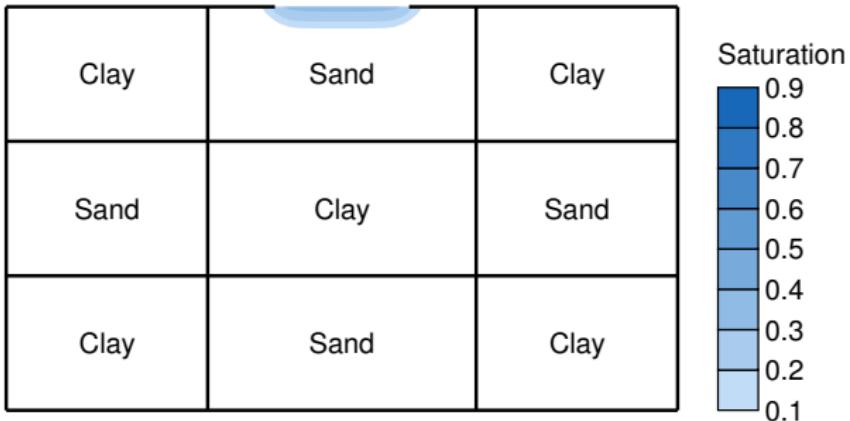
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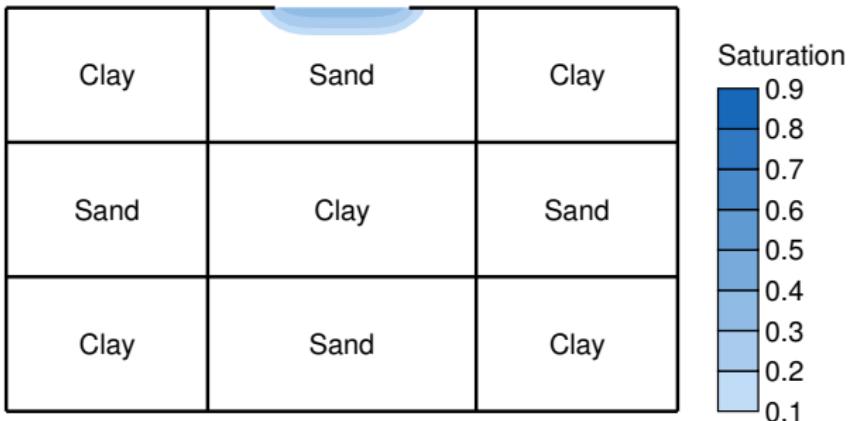
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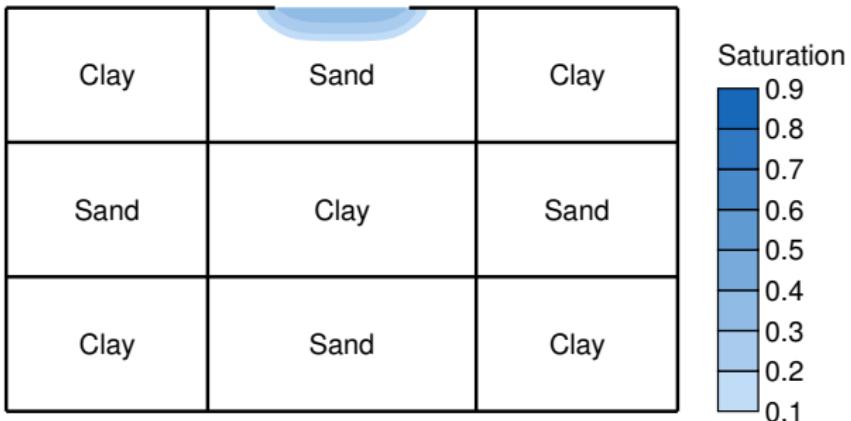
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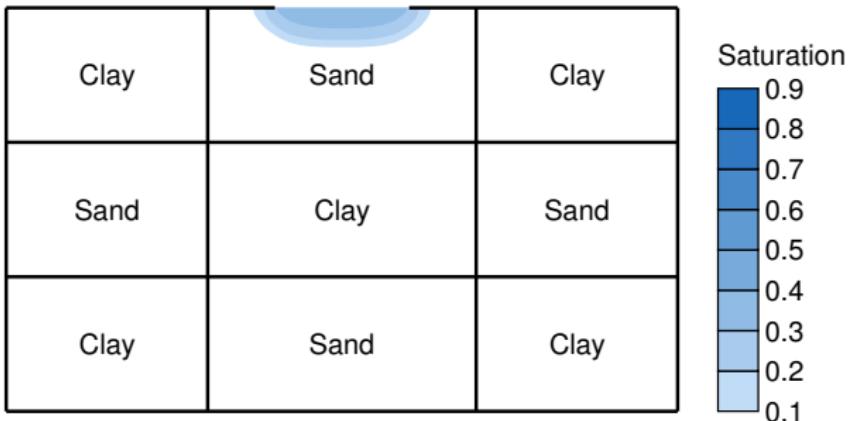
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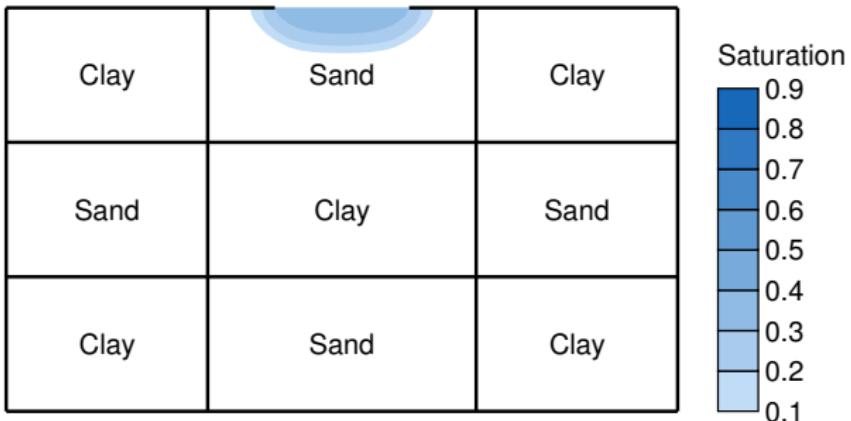
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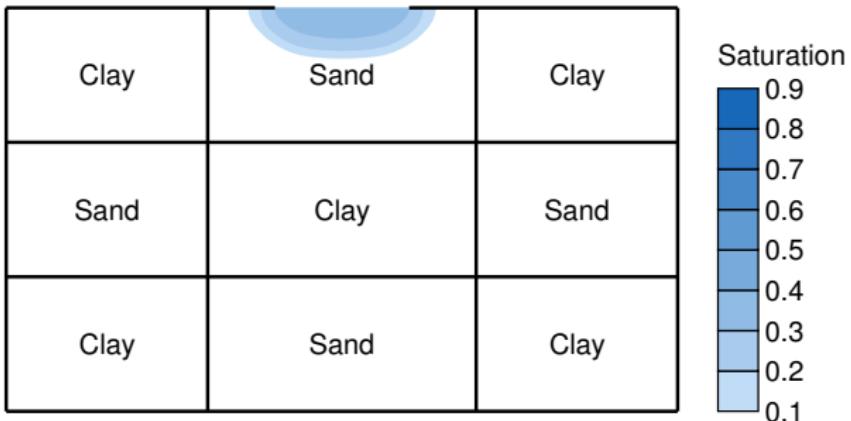
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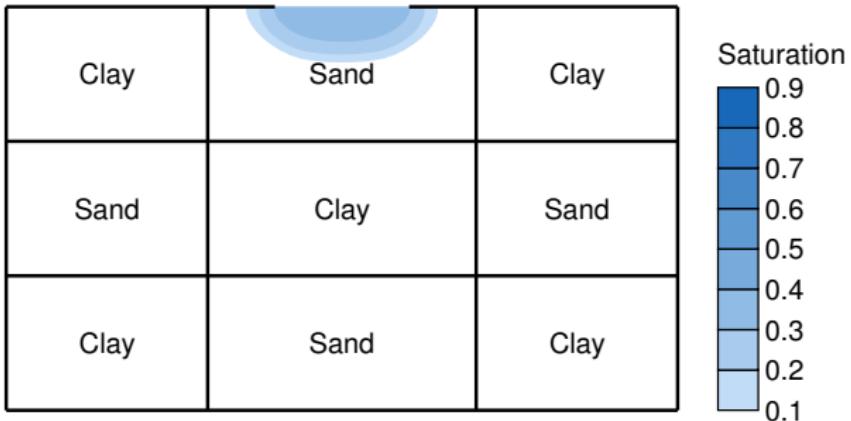
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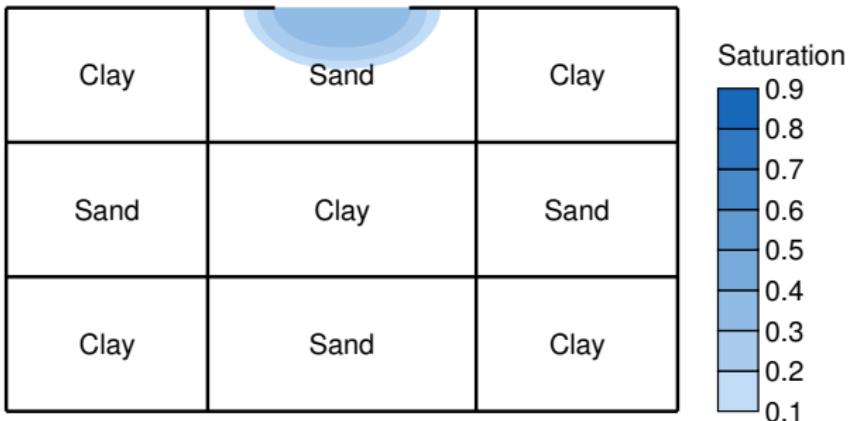
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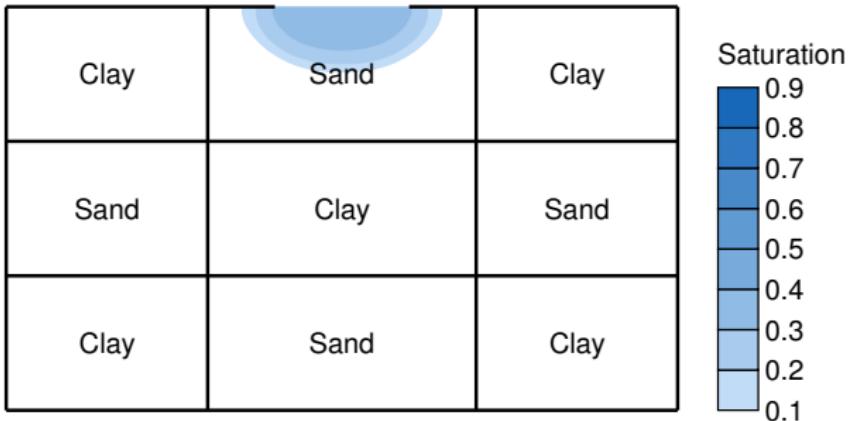
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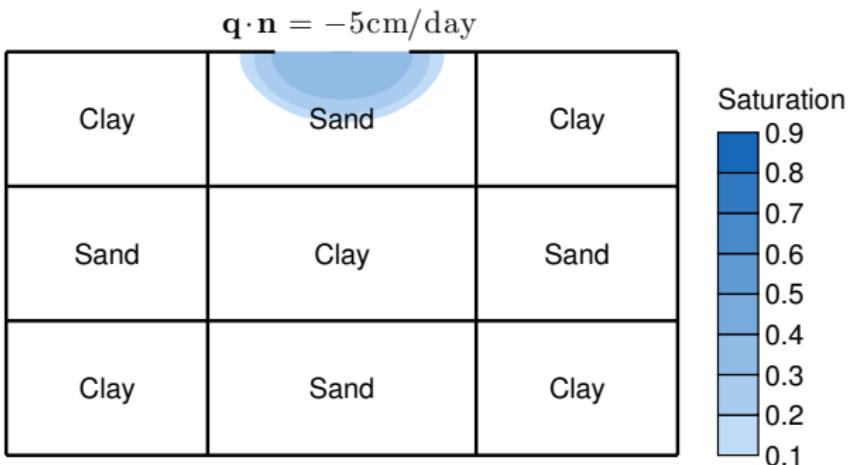


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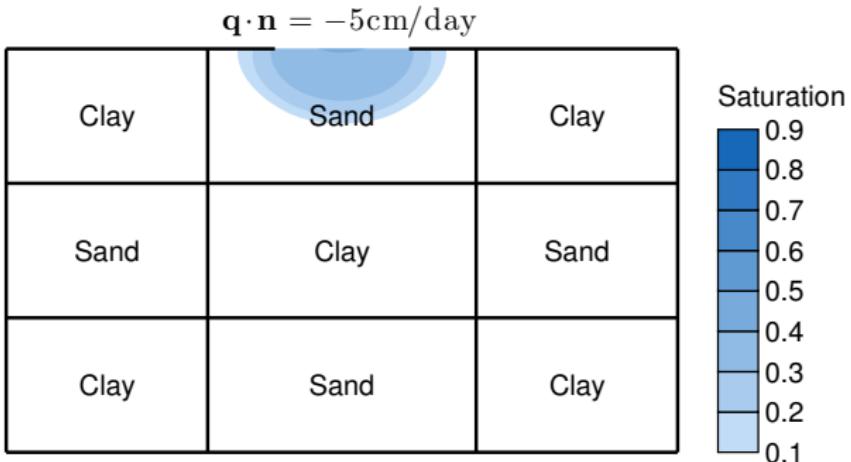
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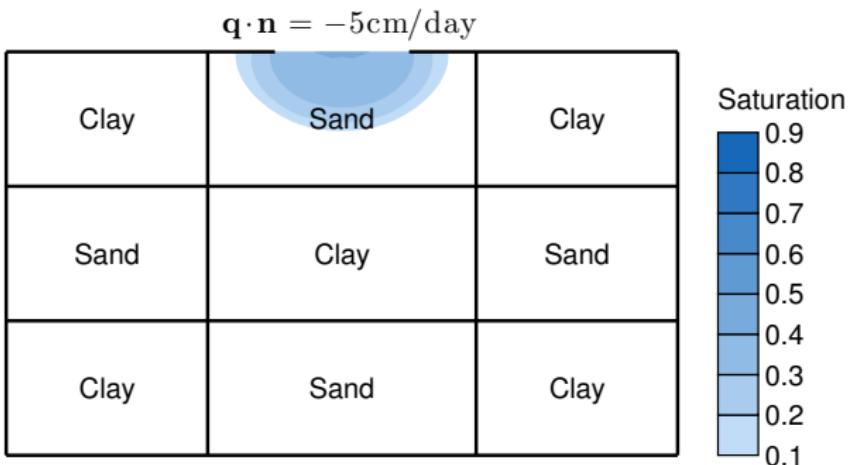
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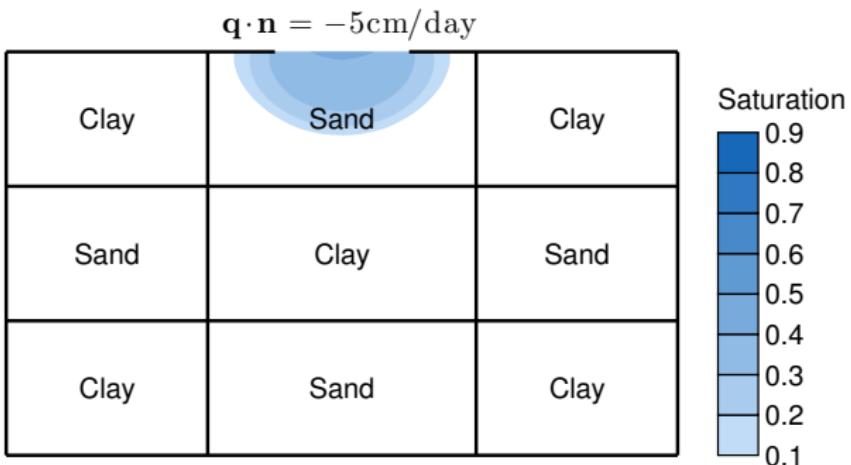
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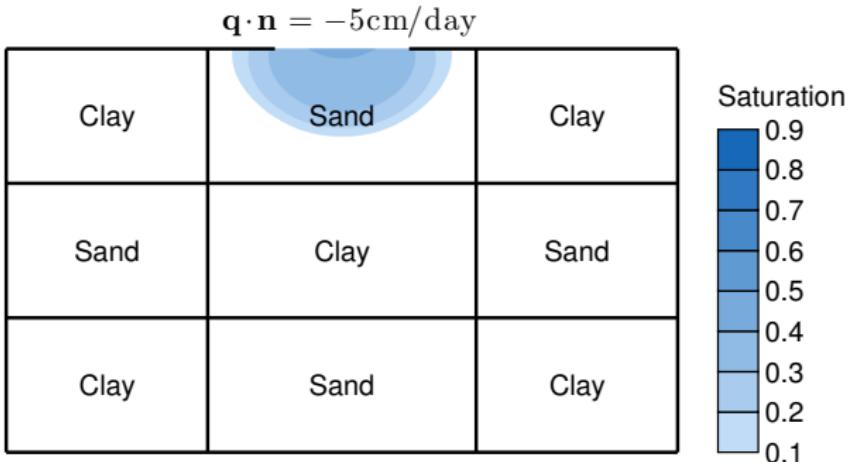
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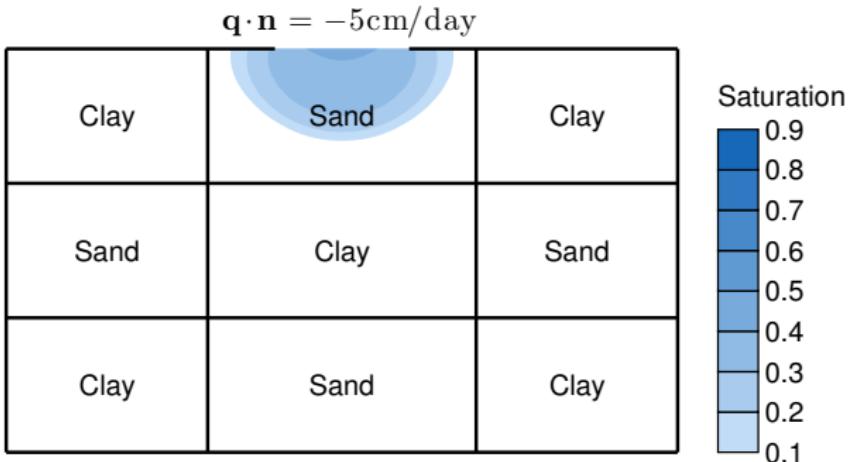
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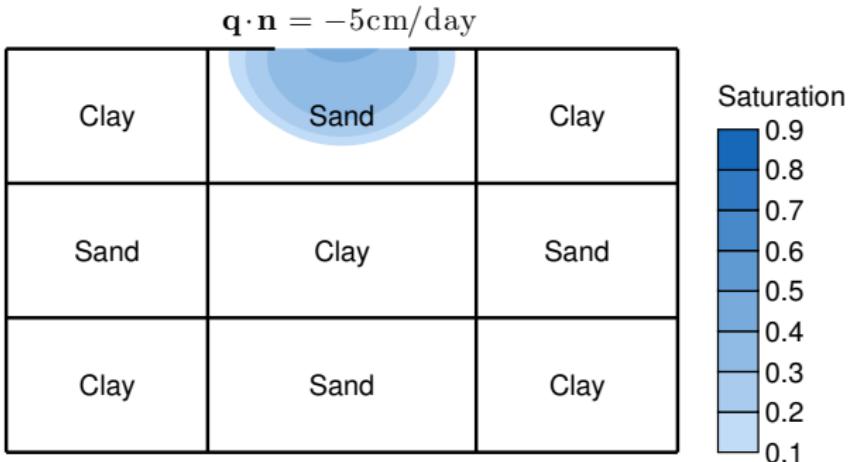
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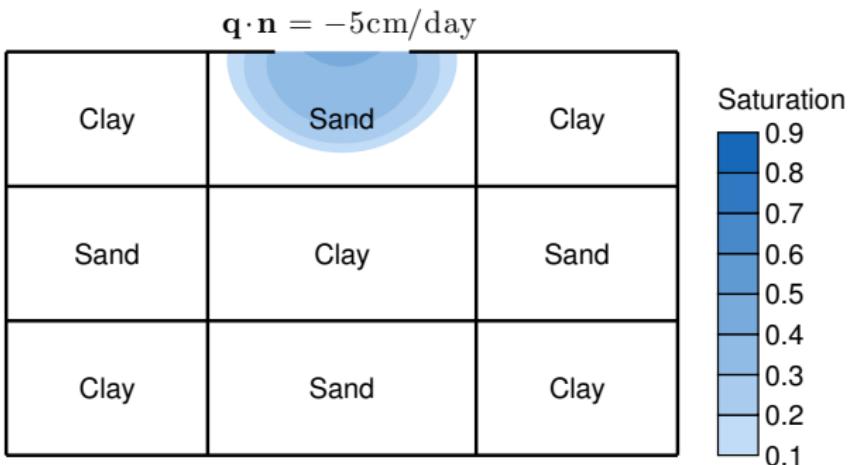
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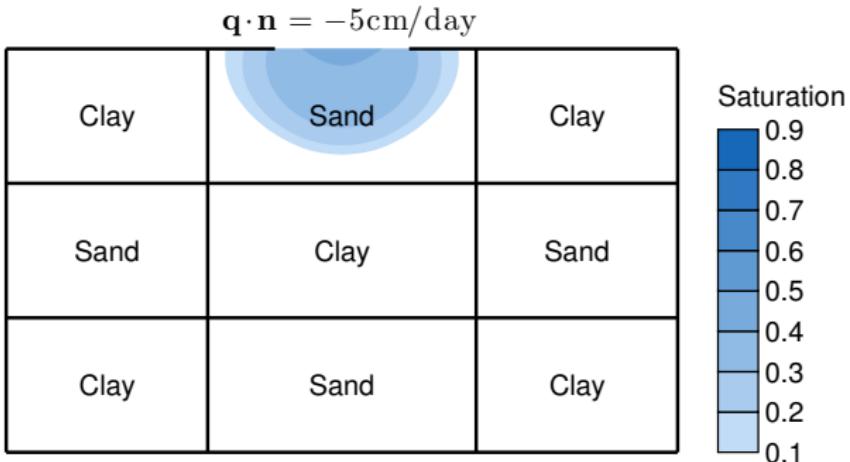
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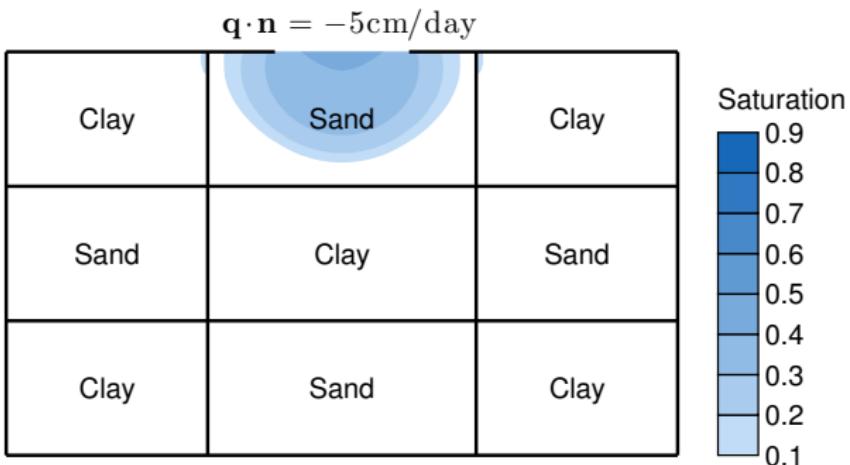
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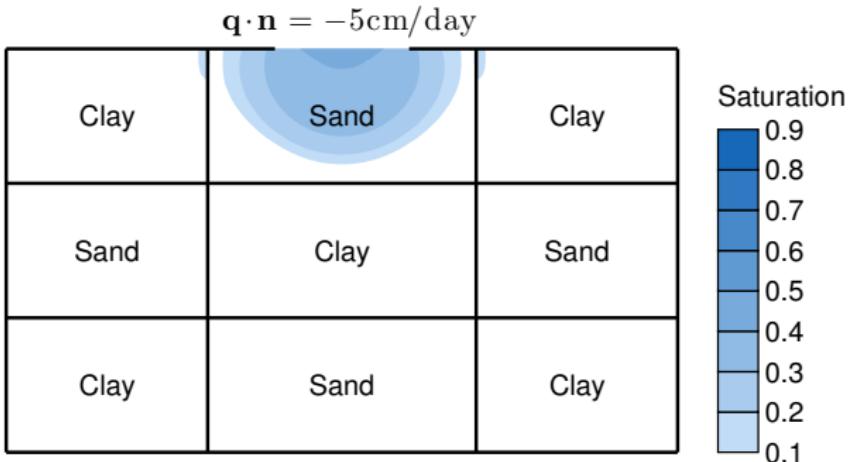
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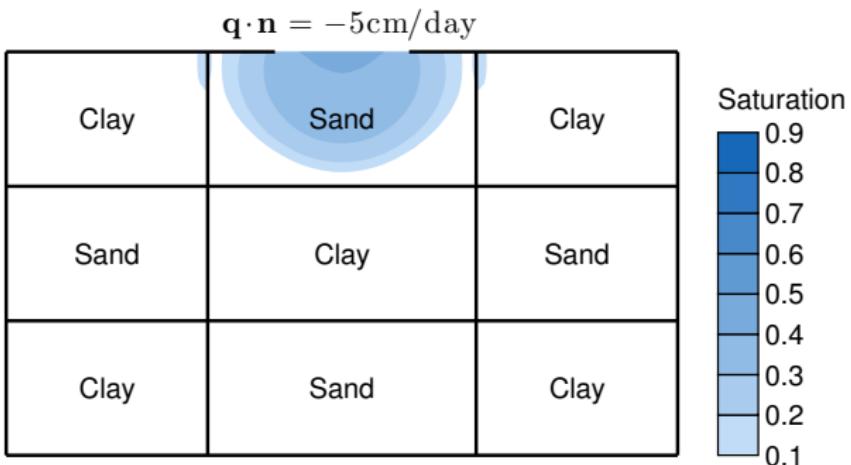
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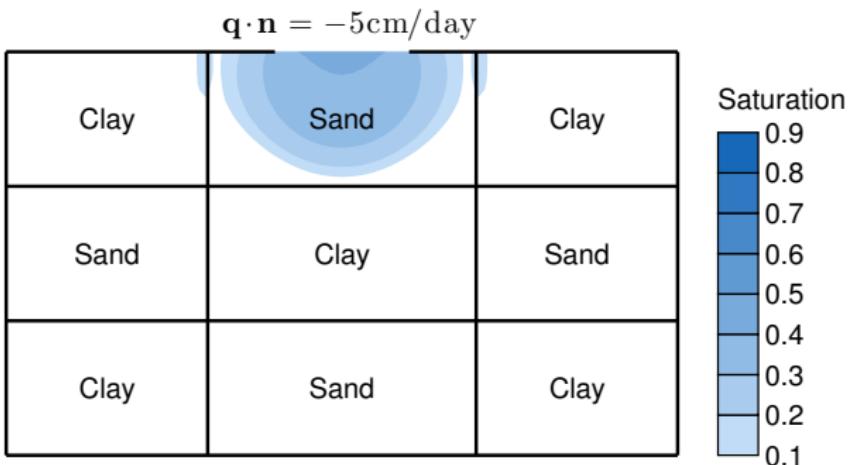
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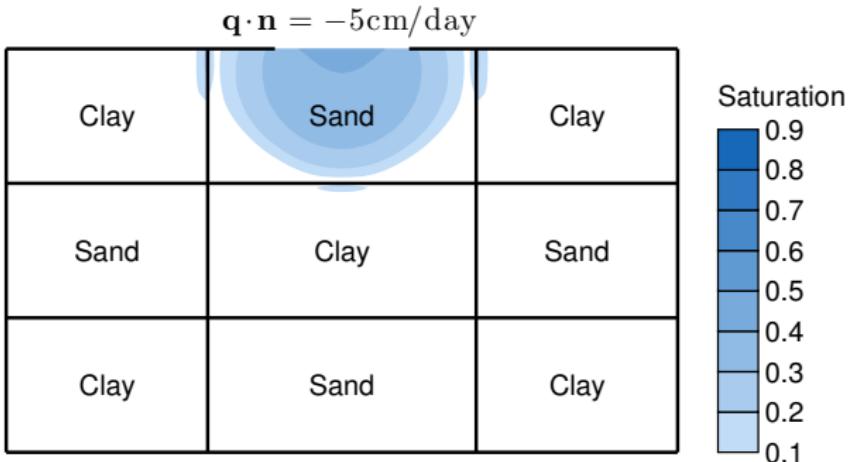
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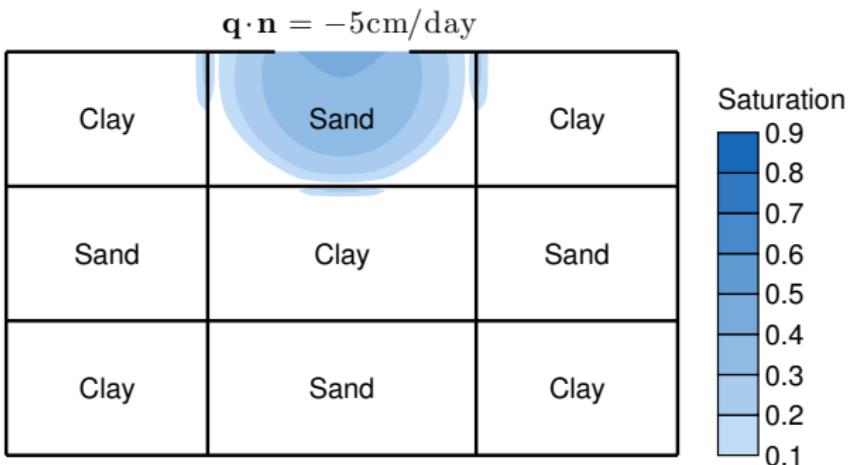
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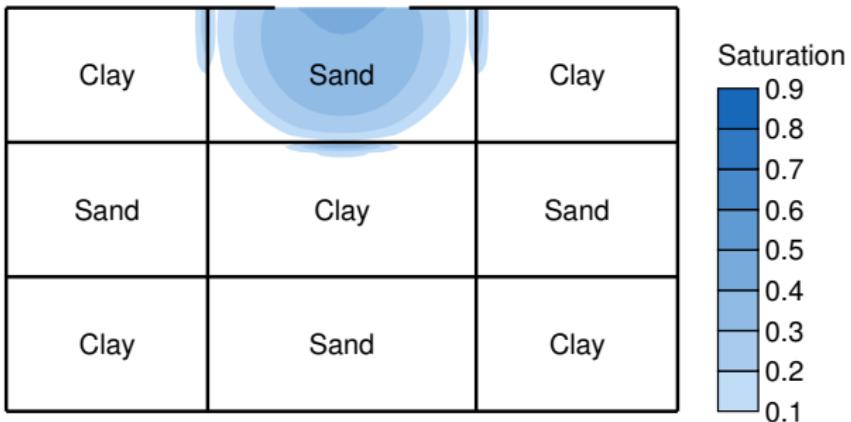


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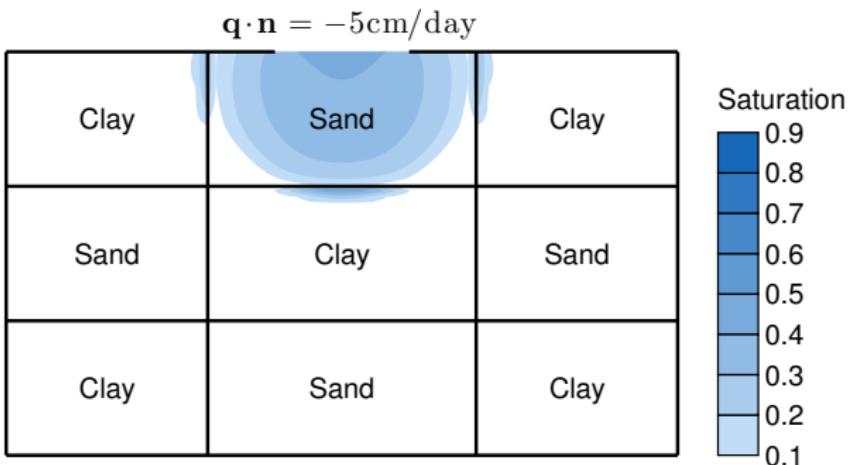


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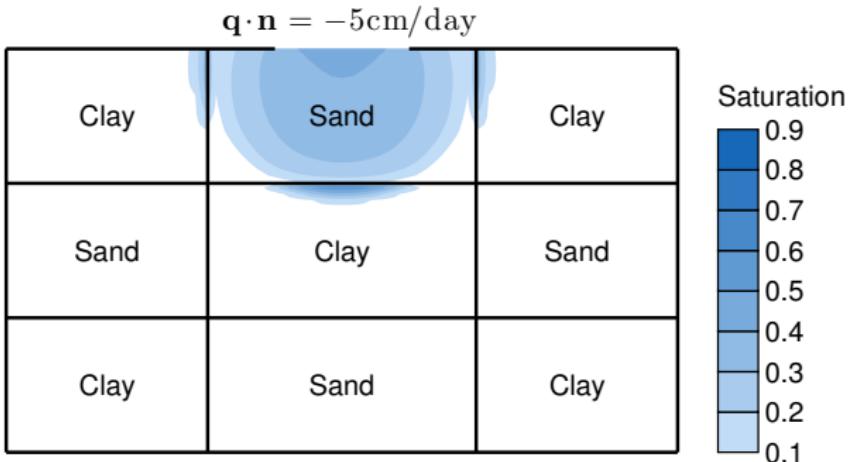
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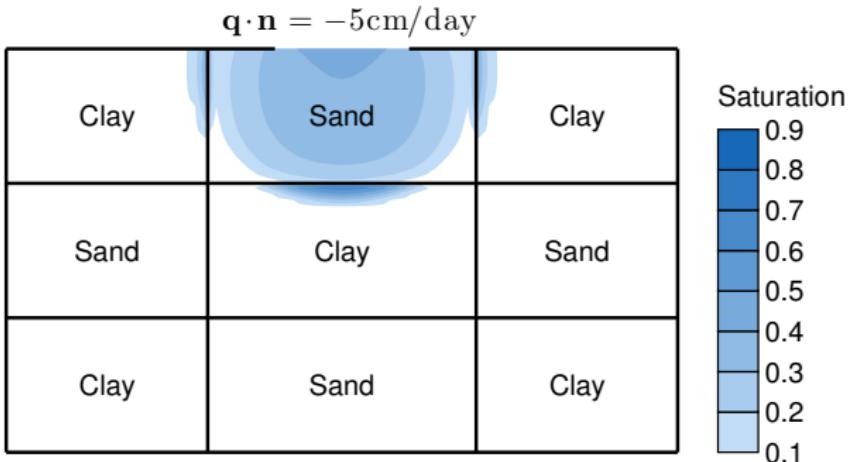
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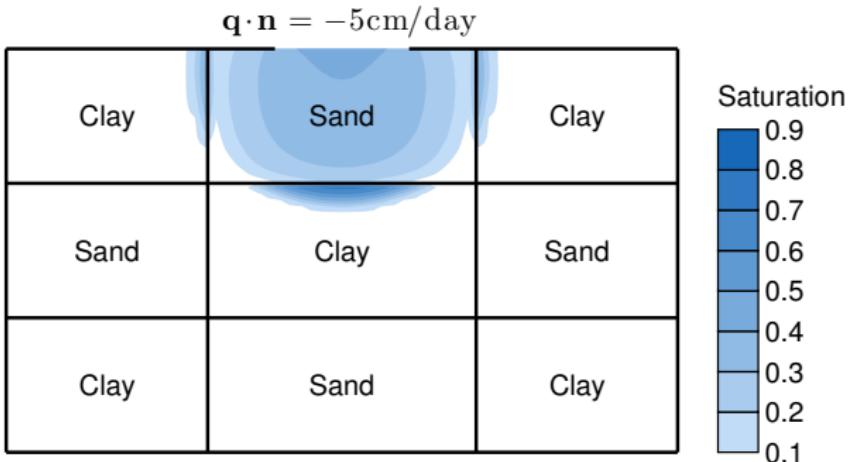
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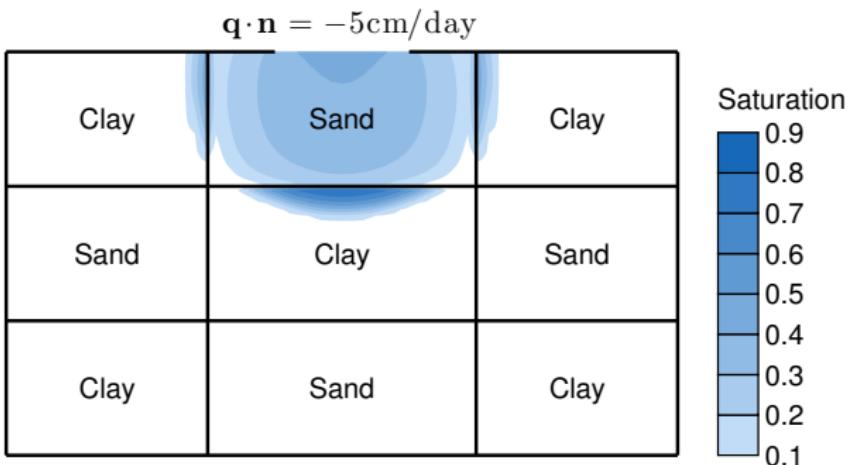
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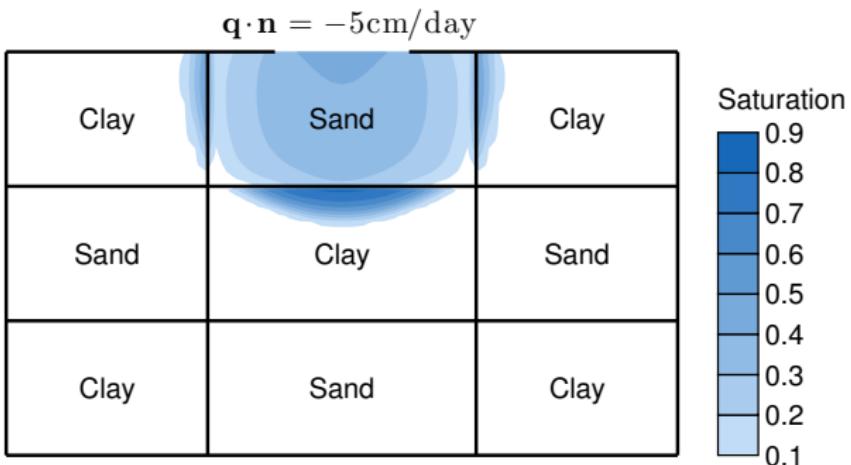
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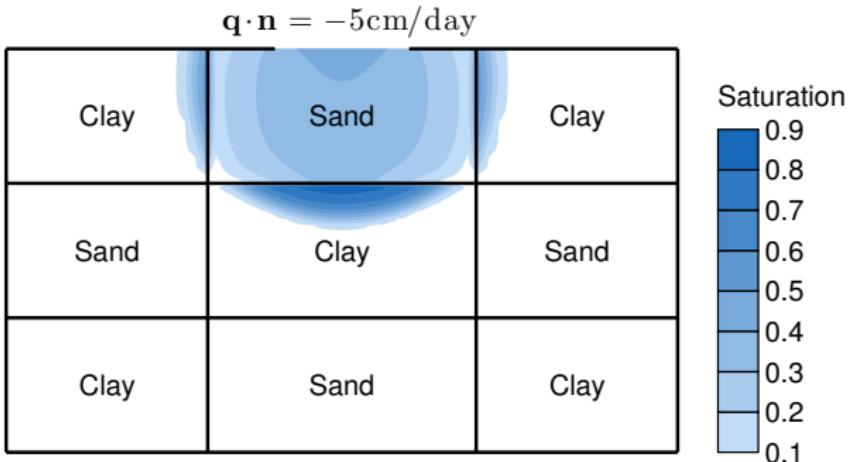
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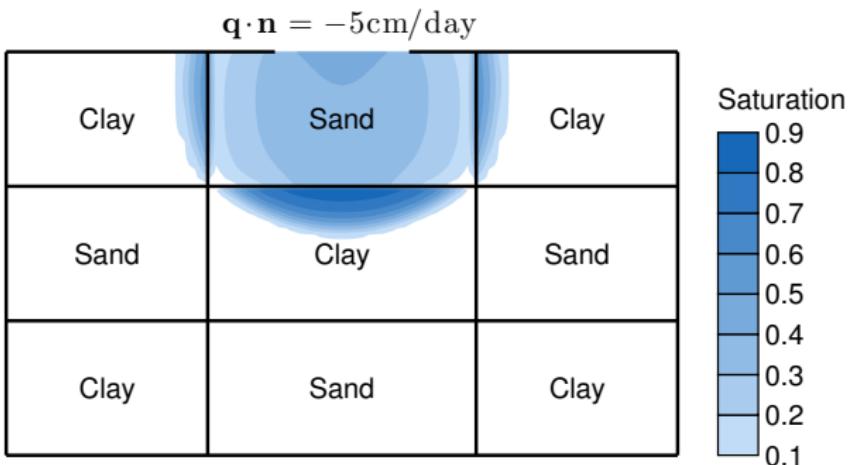
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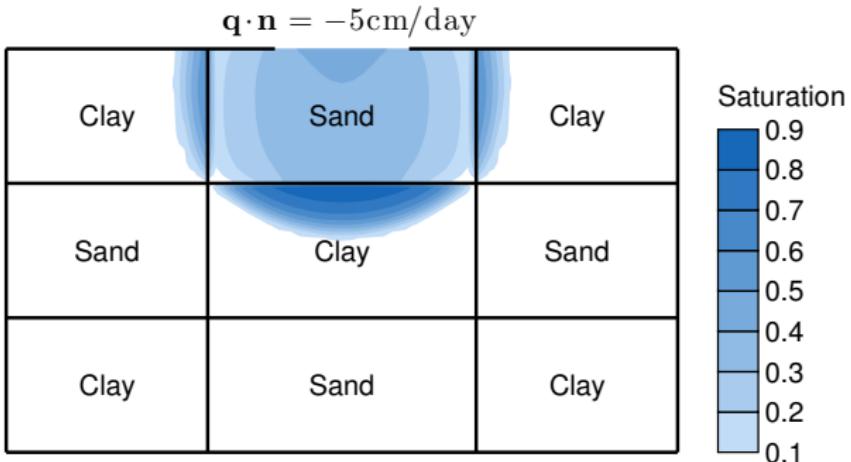
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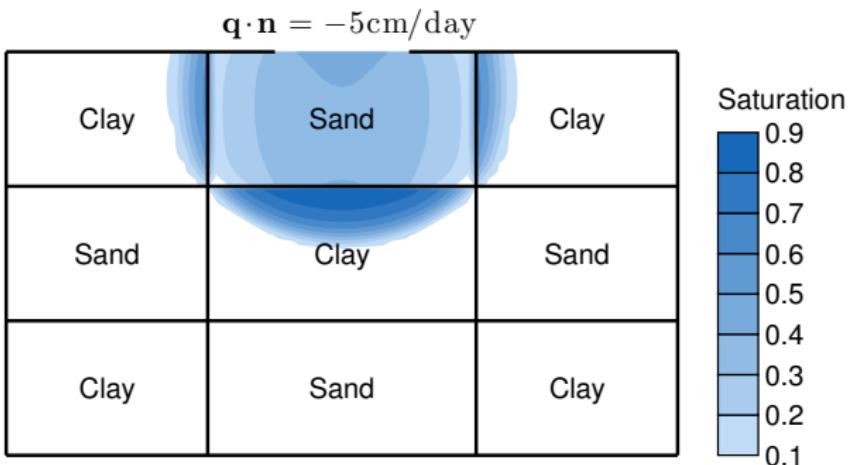
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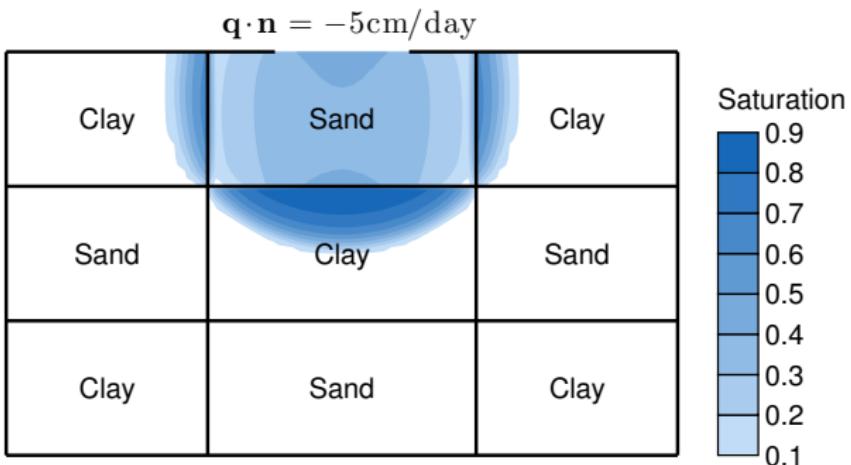
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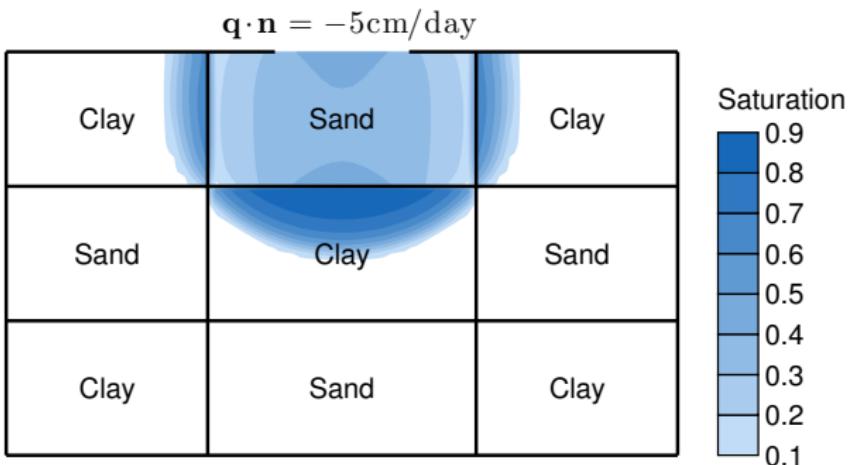
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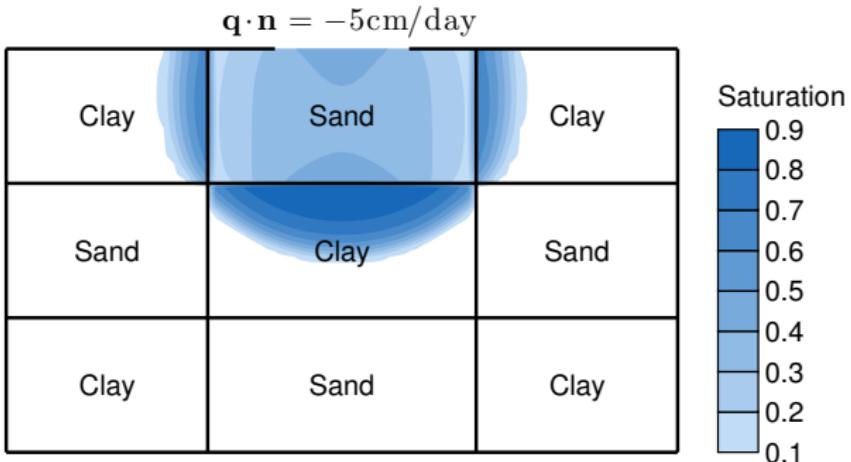
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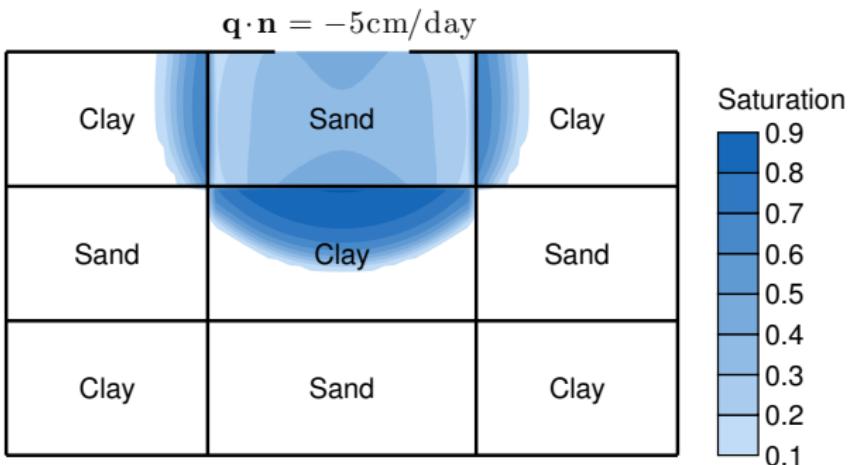
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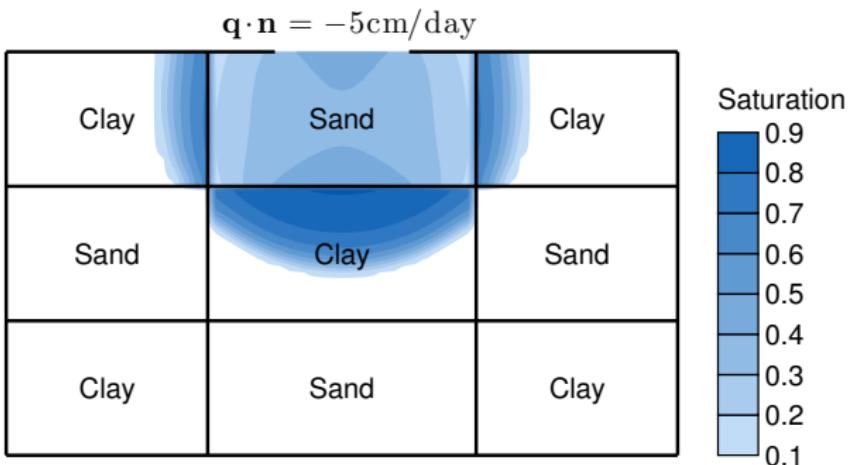
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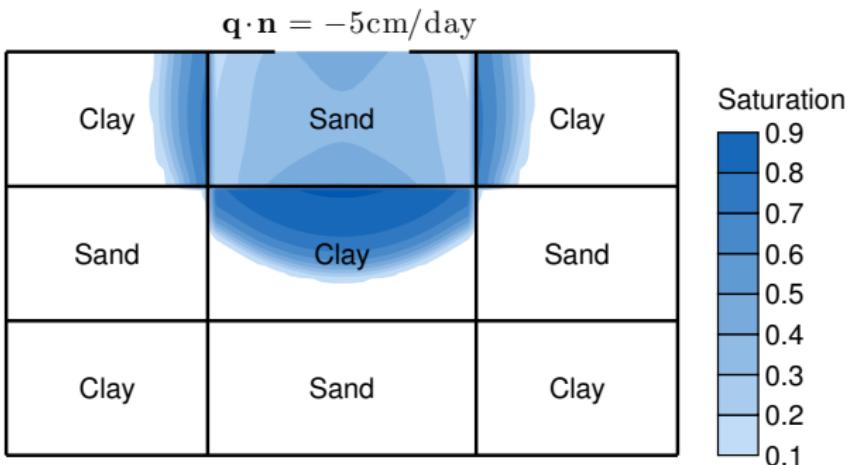
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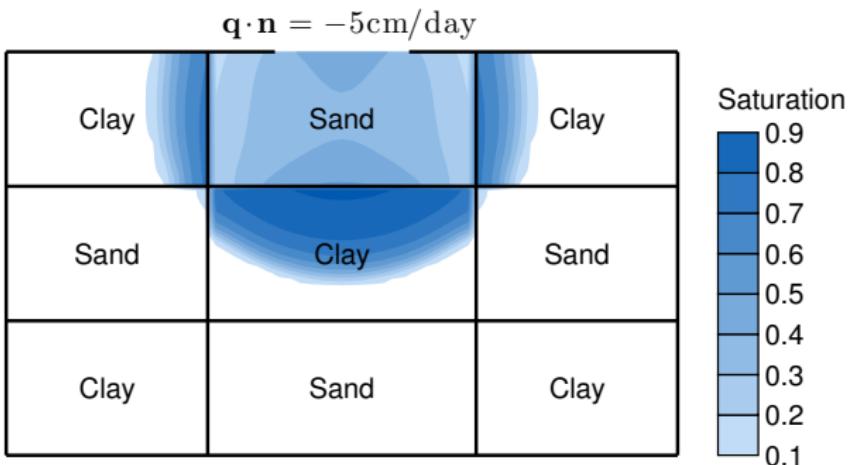
Test Problem: Water infiltration



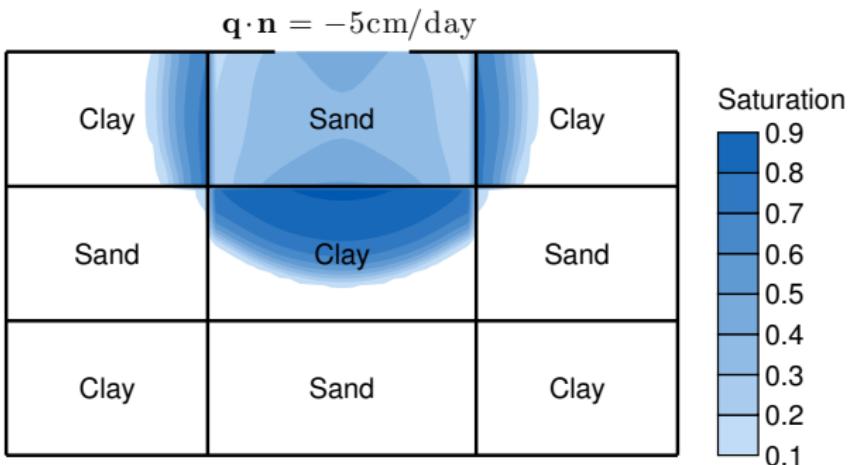
Test Problem: Water infiltration



Test Problem: Water infiltration

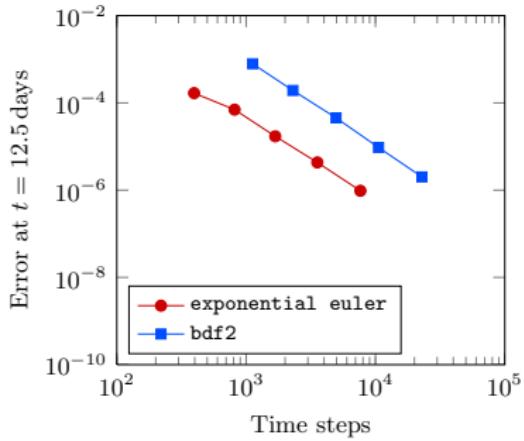
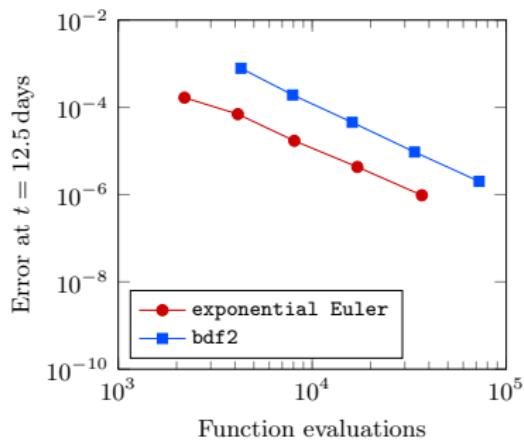


Test Problem: Water infiltration



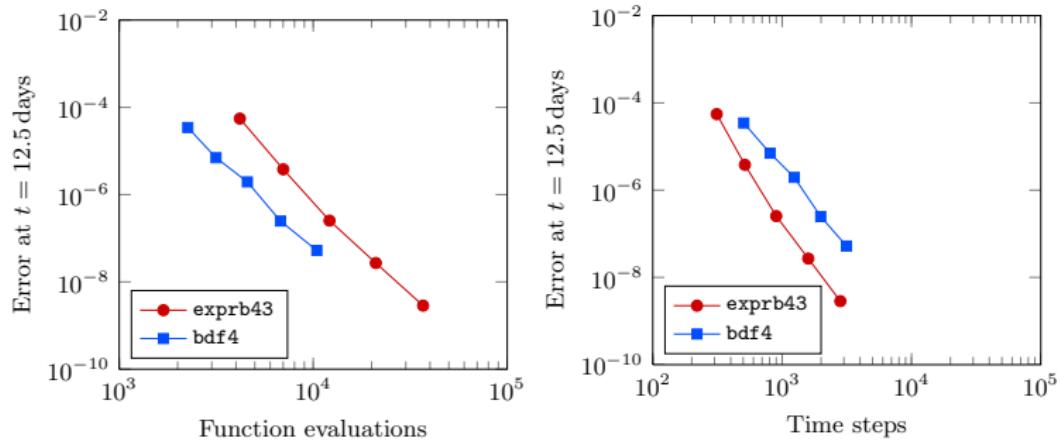
Test Case: Unsaturated water flow

Methods of Order 2



Test Case: Unsaturated water flow

Methods of Order 4



Summary and Conclusions

Pros and Cons of exponential integrators:

- ✓ Krylov subspace methods converge rapidly
- ✓ Implemented efficiently without preconditioning \Rightarrow Jacobian free
- ✓ Good stability properties \Rightarrow Large time steps
- ✗ Spatial discretisation must be expressed in the form of

$$\frac{du}{dt} = \mathbf{g}(u), \quad u(0) = u_0$$

- ✗ Performance declines in terms of function evaluations as we move up in order

Open Problem: Higher order methods require multiple matrix-function vector products with the same Jacobian matrix. How to recycle Krylov subspace information from one subspace to the next?

Overview of Presentation

- ▶ Modelling of unsaturated water flow
- ▶ Time integration methods for unsaturated water flow: Exponential integrators
- ▶ Two-scale numerical modelling of unsaturated water flow in soils exhibiting small-scale heterogeneities

Problem Statement

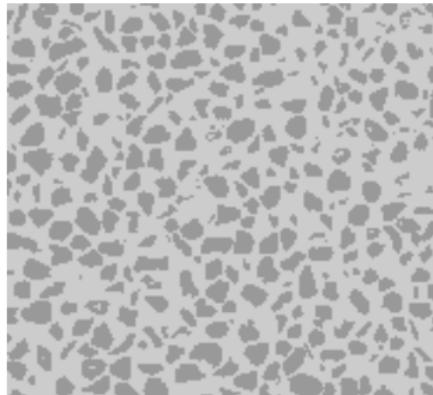
- ▶ Richards' equation in two-dimensions

$$\frac{\partial}{\partial t} \theta(h) + \nabla \cdot [-K(h) \nabla (h + x_2)] = 0$$

- ▶ Domain comprised of two sub-domains Ω_a (connected) and Ω_b (disconnected) with different hydraulic properties:

$$\theta(h) = \begin{cases} \theta_a(h) & \text{in } \Omega_a \\ \theta_b(h) & \text{in } \Omega_b \end{cases}$$

$$K(h) = \begin{cases} K_a(h) & \text{in } \Omega_a \\ K_b(h) & \text{in } \Omega_b \end{cases}$$



Heterogeneous domain

Ω_a ■ Ω_b ■

- ▶ Computational cost of direct numerical simulation is prohibitively expensive when the domain exhibits small-scale heterogeneity.

Two-scale Model for unsaturated flow

- ▶ Macroscopic equation ($x \in \Omega$)

$$\frac{\partial}{\partial t} \theta_{\text{eff}}(h_a) + \nabla_x \cdot [-\mathbf{K}_{\text{eff}}(h_a) \nabla_x (h_a + x_2)] = Q$$

- ▶ Microscopic equation ($y \in \Omega_{x,b}$)

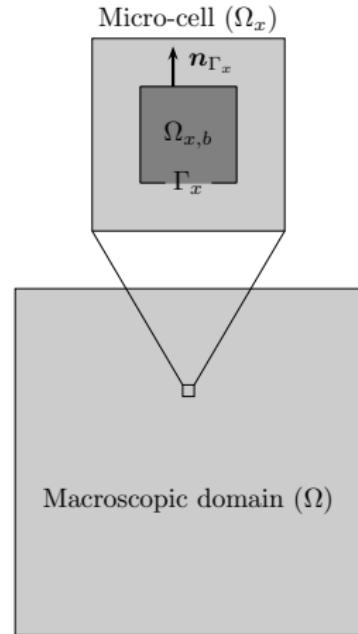
$$\frac{\partial}{\partial t} \theta_b(h_b) + \nabla_y \cdot [-K_b(h_b) \nabla_y (h_b + y_2)] = 0$$

- ▶ Microscopic boundary condition ($y \in \Gamma_x$)

$$h_a = h_b$$

- ▶ Source term

$$Q = \frac{1}{|\Omega_x|} \int_{\Gamma_x} -K_b(h) \nabla_y (h_b + y_2) \cdot \mathbf{n}_{\Gamma_x} \, ds$$



See, e.g., Szymkiewicz and Lewandowska (2006).

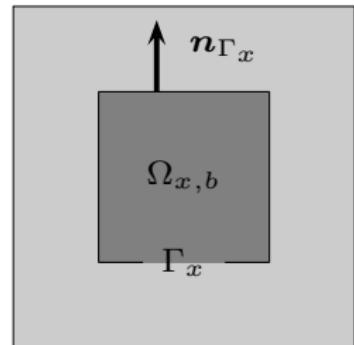
Effective hydraulic conductivity

- $(\mathbf{K}_{\text{eff}})_{*,j}$ is a matrix with j th column equal to

$$(\mathbf{K}_{\text{eff}})_{*,j} = \frac{1}{|\Omega_x|} \int_{\Omega_{x,a}} K_a(h_a) \nabla_y (u + y_2) \, dA$$

where u is a solution of the periodic cell-problem:

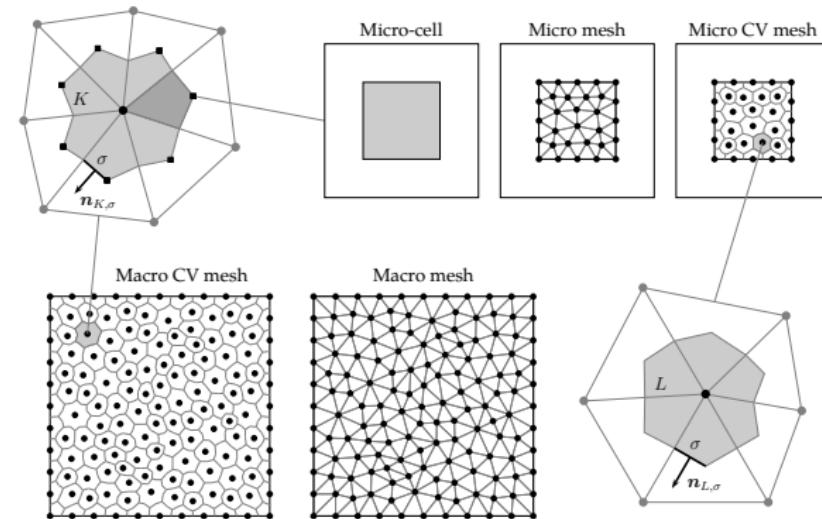
$$\begin{cases} \nabla_y \cdot (K_a(h_a) \nabla_y (u + y_2)) = 0 & y \in \Omega_{x,a} \\ K_a(h_a) \nabla_y (u + y_2) \cdot \mathbf{n}_{\Gamma_x} = 0 & y \in \Gamma_x \\ u \text{ is } \Omega_x\text{-periodic} & \end{cases}$$



- Pre-processing step:
 - Compute entries of \mathbf{K}_{eff} using a range of values of h_a
 - Use interpolation to evaluate \mathbf{K}_{eff} at any value of h_a

Unstructured CV spatial discretisation

- Unstructured vertex-centered CV method [Carr and Turner (2014)]



- Existing numerical strategies (e.g., Szymkiewicz and Lewandowska (2008)) only applicable to simple inclusion geometries

Meshing of micro-cells

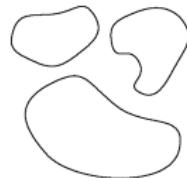
Image-based meshing code built on GMSH [[Guezaine and Remacle \(2009\)](#)]



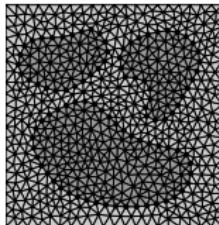
Bitmap image



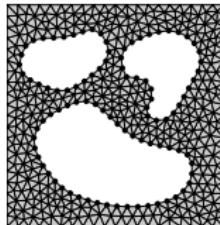
Binary image



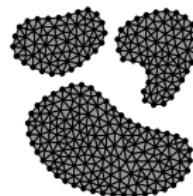
Edge detection



Full micro-cell



Ω_a only



Ω_b only

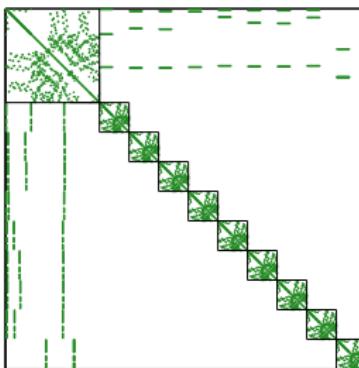
Spatially-discrete system of ODEs

- ▶ Spatial discretisation can be expressed in the form

$$\frac{d\mathbf{u}}{dt} = \mathbf{g}(\mathbf{u}), \quad \mathbf{u}(0) = \mathbf{u}_0 \in \mathbb{R}^N,$$

where $N = \text{num_macro_nodes} + \text{num_macro_elements} \times \text{num_micro_nodes}$.

- ▶ Example sparsity structure of Jacobian matrix (zoomed in)



$$\mathbf{J}(\mathbf{u})\mathbf{v} \approx [\mathbf{g}(\mathbf{u} + \varepsilon\mathbf{v}) - \mathbf{g}(\mathbf{u})]/\varepsilon$$

- ▶ Time integration: Jacobian-free exponential Euler method [Carr et al. (2011)]

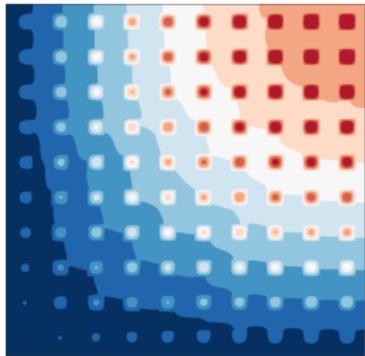
Code implementation details

- ▶ Code developed in C++
- ▶ Linear algebra operations performed using BLAS and LAPACK libraries:
 - (a) Intel MKL (HPC Platform)
 - (b) Accelerate framework (Macbook Pro)
- ▶ ODE right-hand side function $g(u)$ implemented in parallel using OpenMP

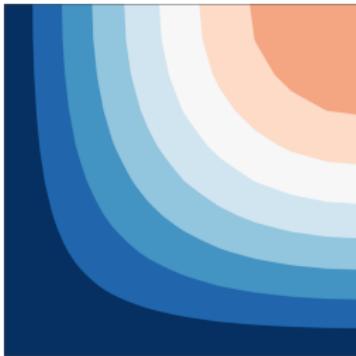
```
#include <omp.h>
omp_set_num_threads(NUM_THREADS);
#pragma omp parallel for
for (k=0; k<num_macro_elements; k++)
{
    ...
}
```

- ▶ Code accommodates both triangular and quad elements at both scales

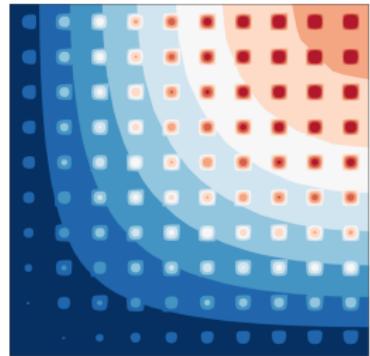
Test Case: Diffusion equation



Full Model
(15 mins)



Macroscopic Model
(1 sec)

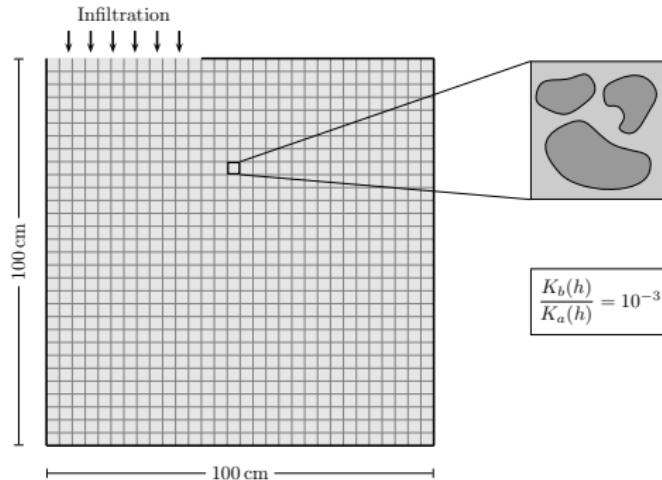


Two-scale Model
(20 secs)

Mesh details:

- ▶ Full Model: 400×400 grid, $N = 160,801$
- ▶ Macroscopic Model: 20×20 grid, $N = 441$
- ▶ Two-scale Model: Macro (20×20 grid), Micro (10×10 grid), $N = 48,841$

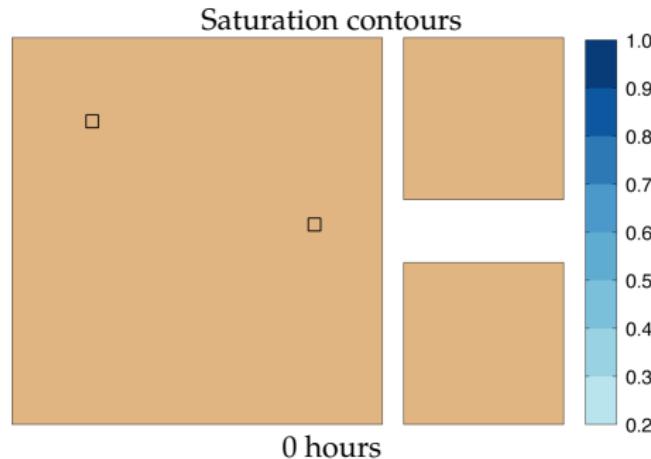
Simulation: Unsaturated water flow



Mesh details:

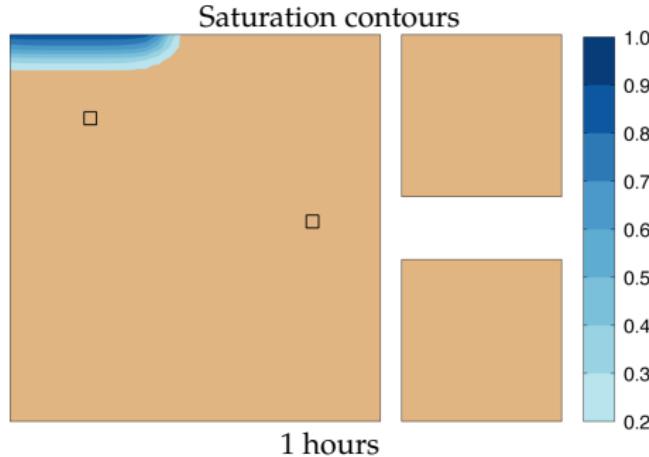
- ▶ Macroscopic mesh (structured): 30×30 grid, 961 nodes
- ▶ Microscopic mesh (unstructured): 532 elements, 316 nodes
- ▶ Total number of unknowns: $N = 961 + 900 \times 316 = 285,361$

Simulation: Unsaturated water flow



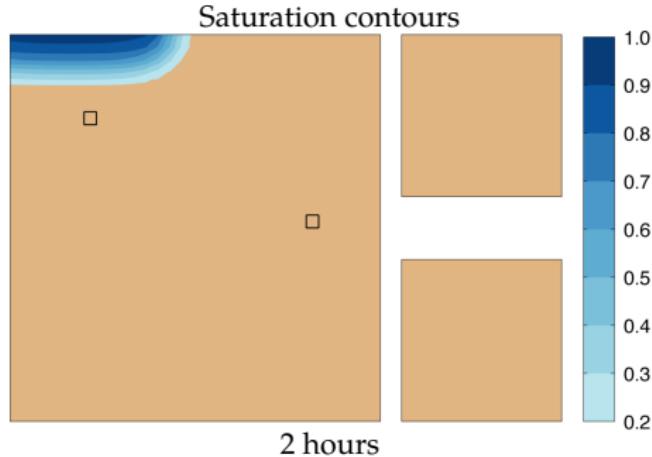
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



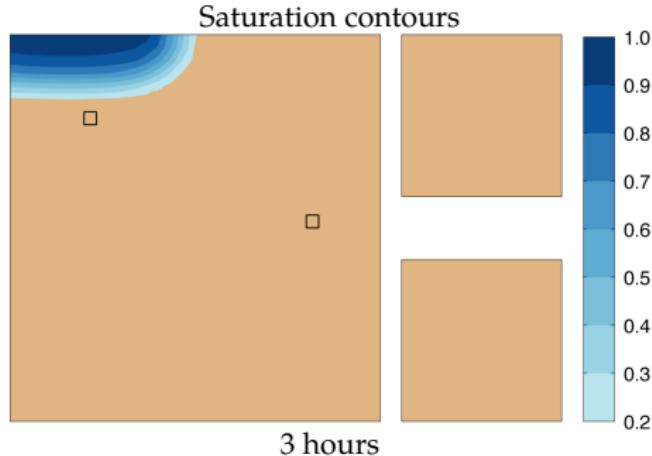
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Simulation: Unsaturated water flow



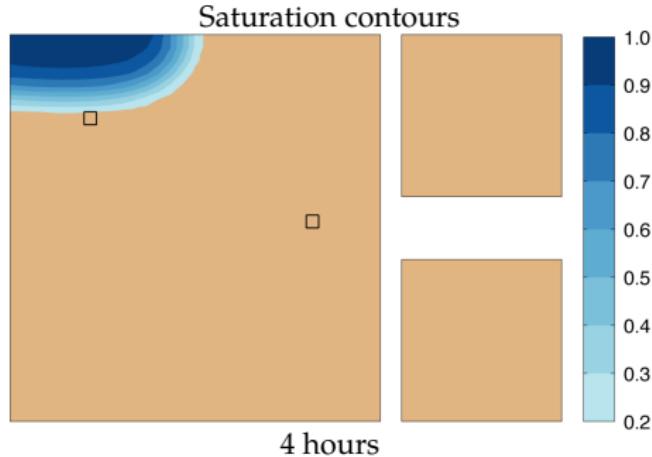
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Simulation: Unsaturated water flow



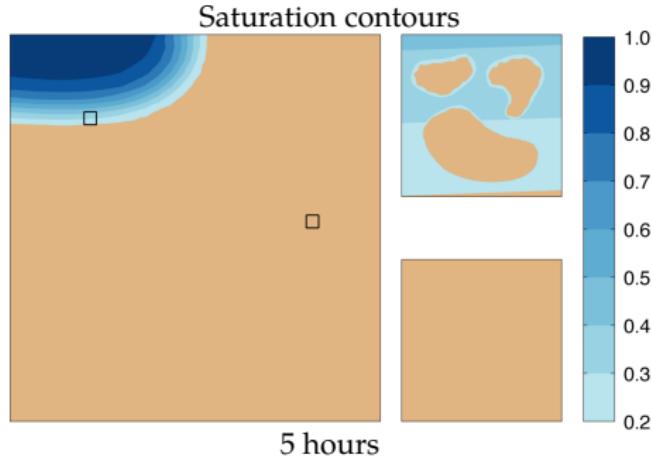
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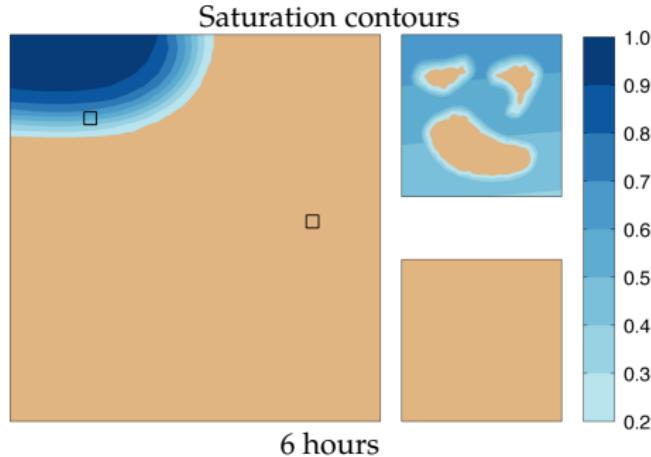
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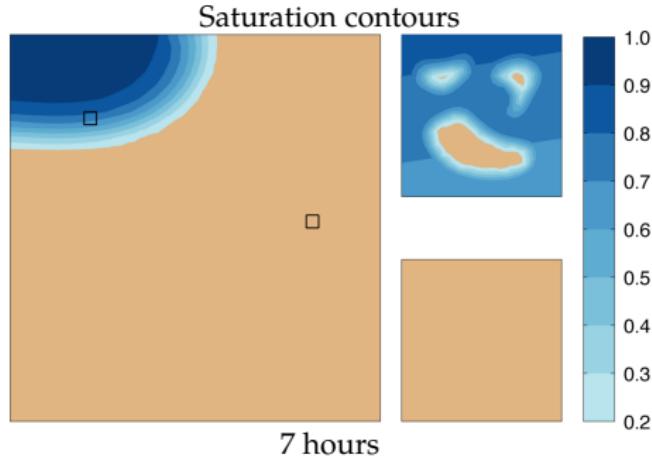
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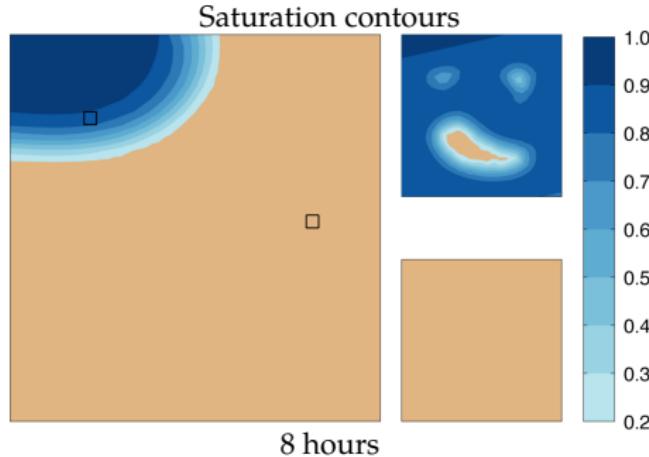
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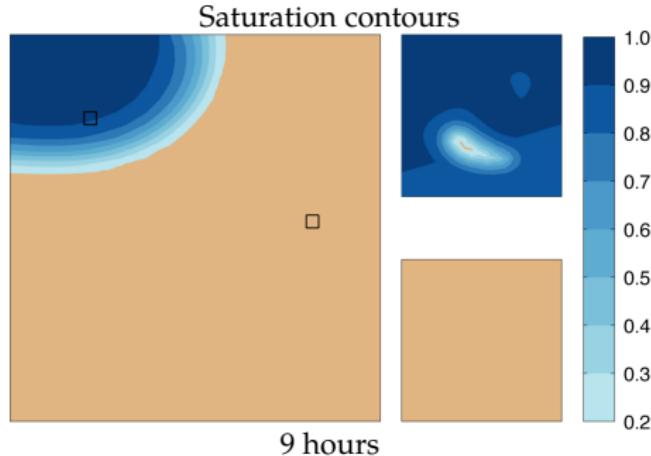
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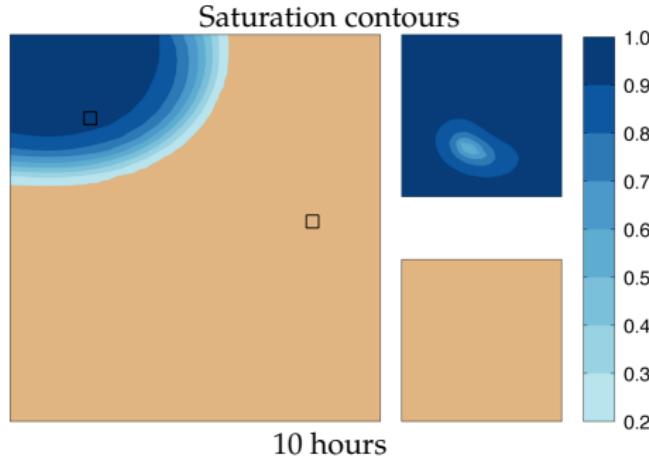
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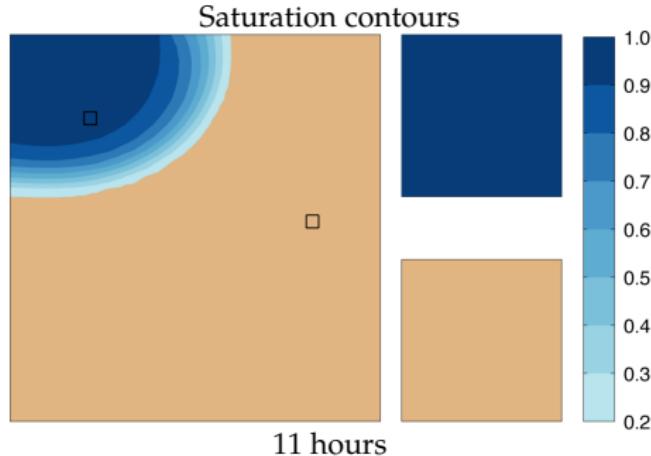
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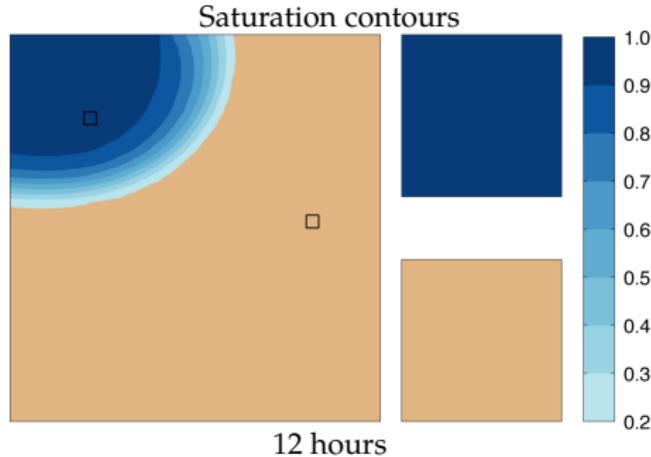
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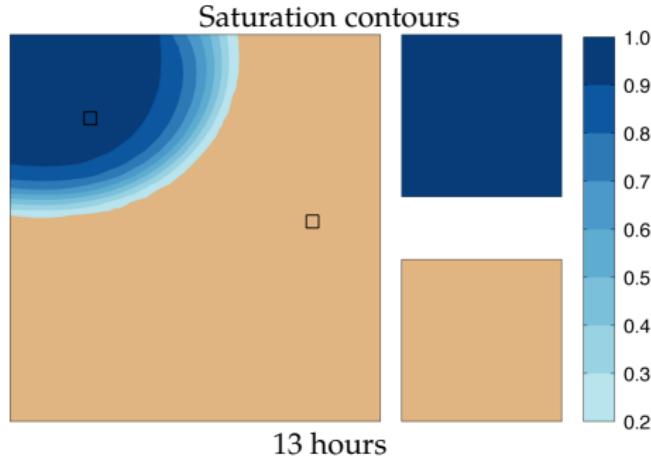
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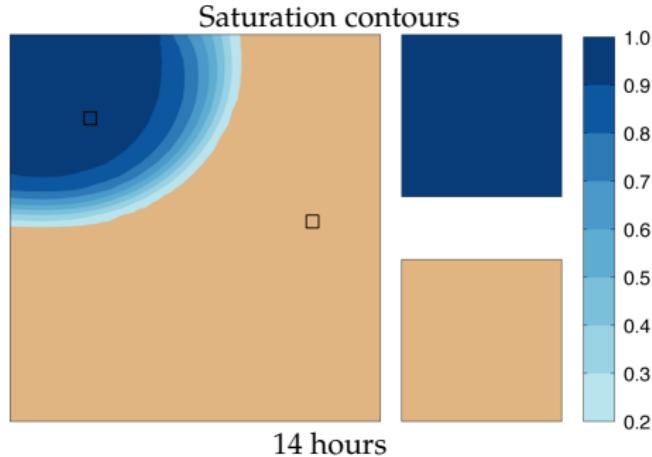
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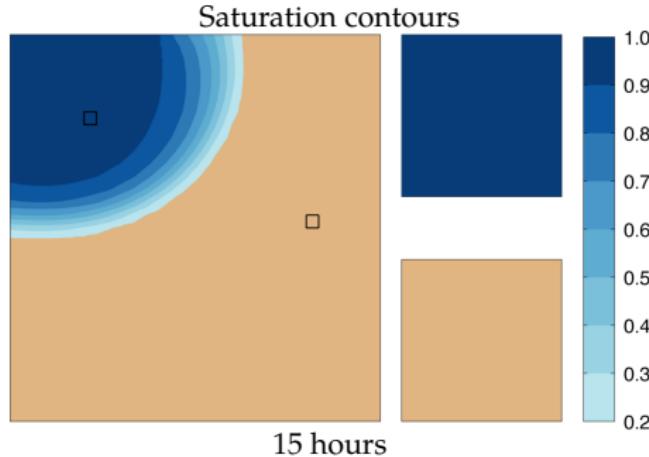
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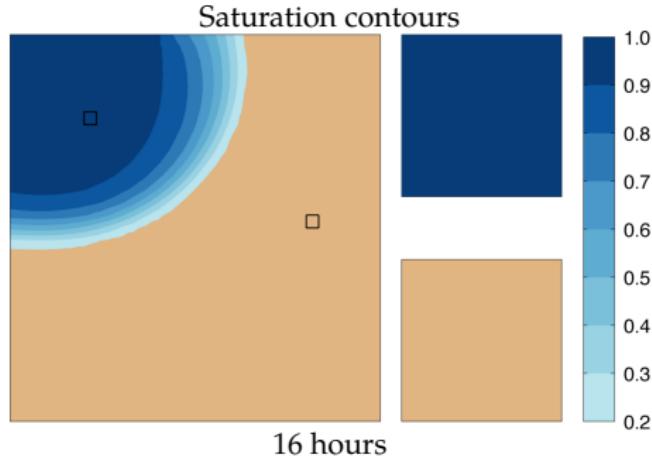
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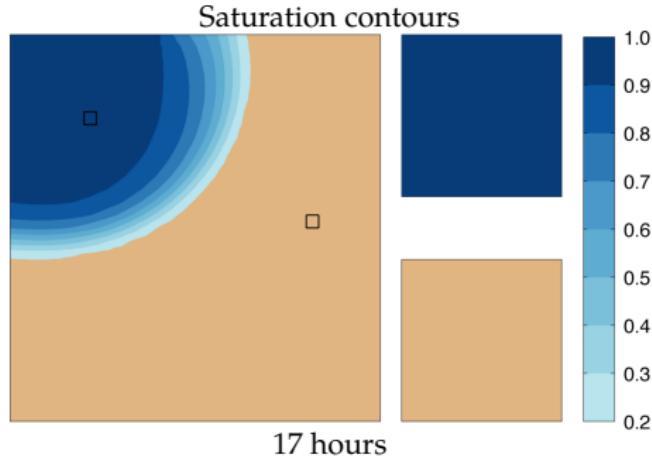
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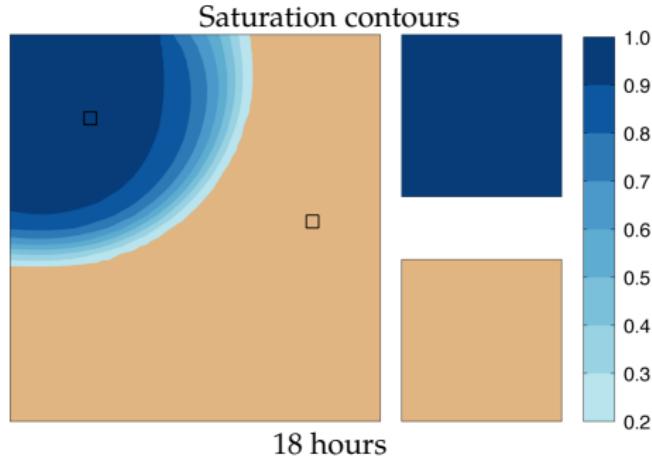
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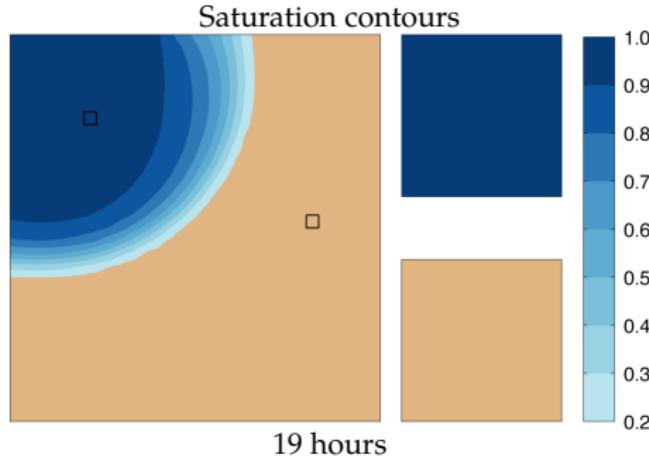
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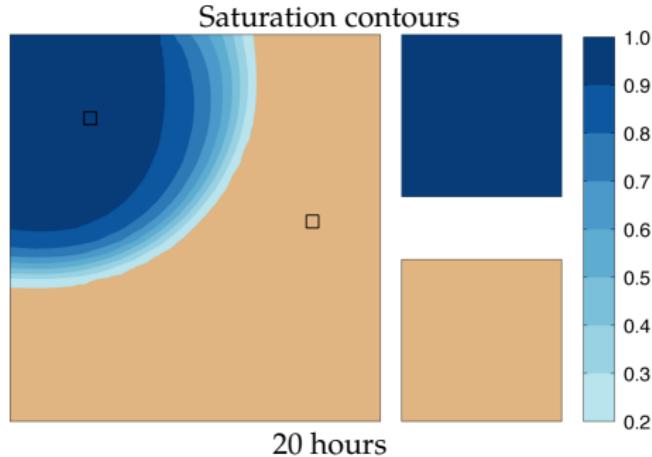
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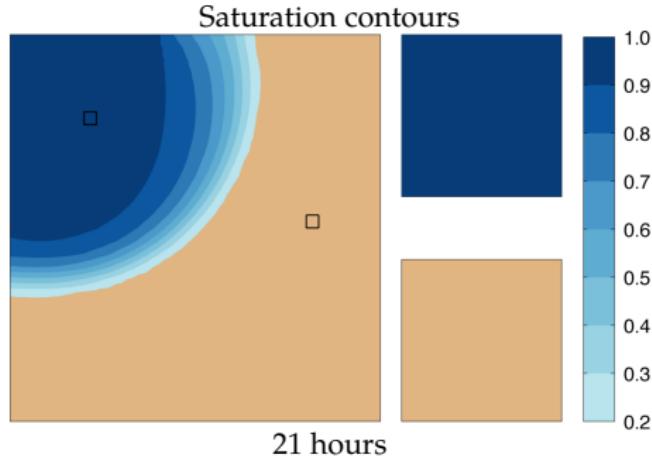
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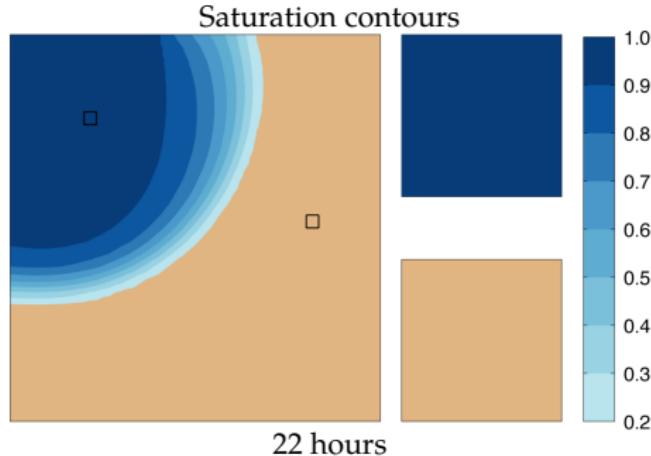
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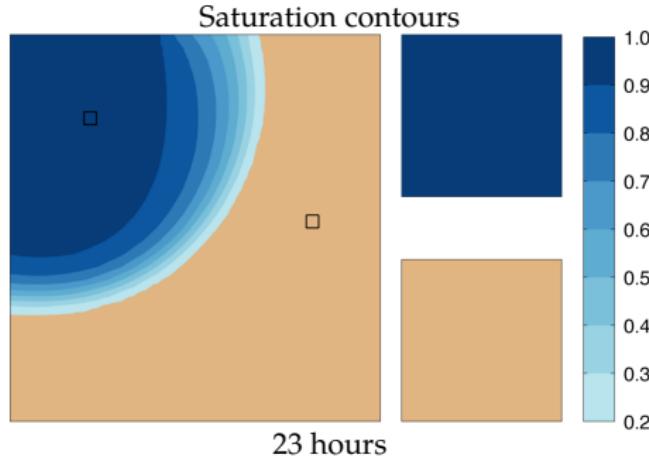
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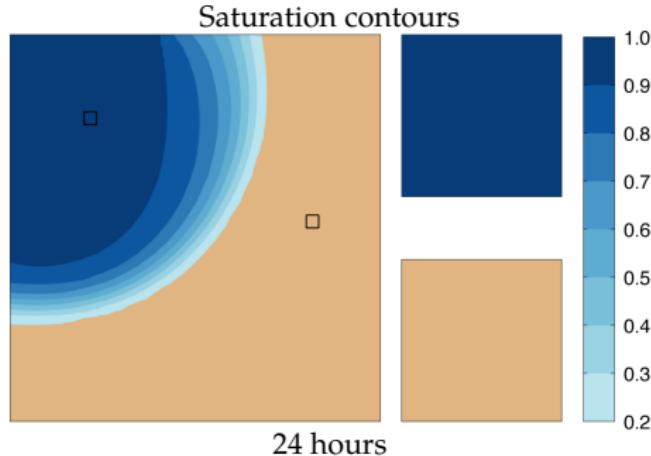
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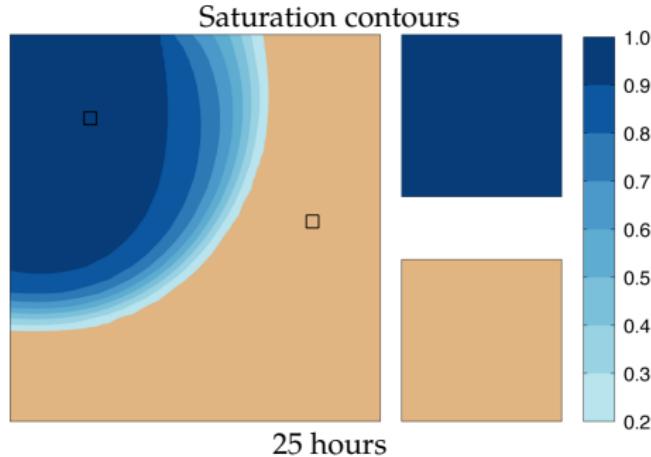
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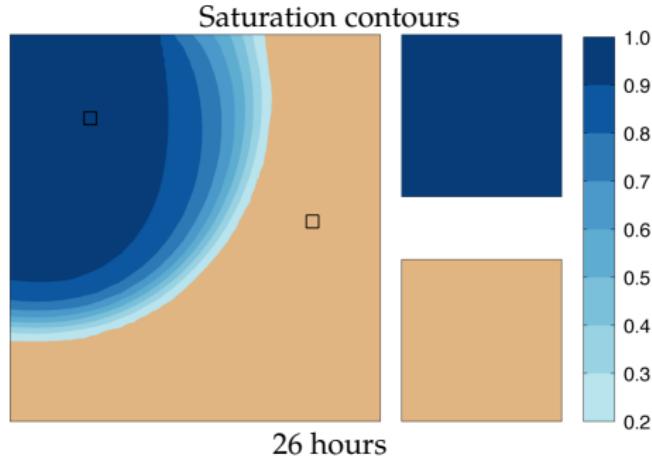
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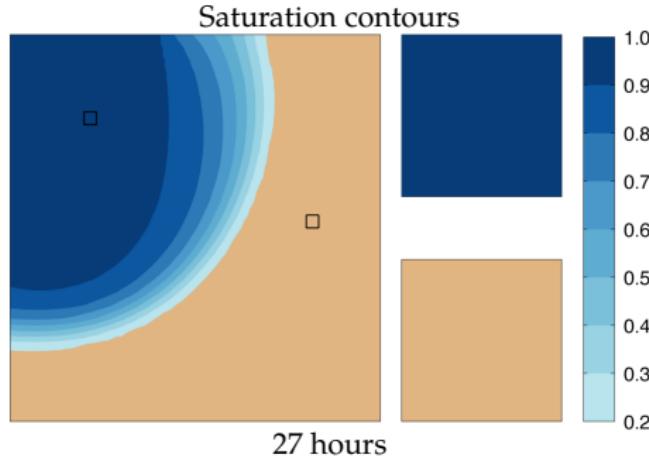
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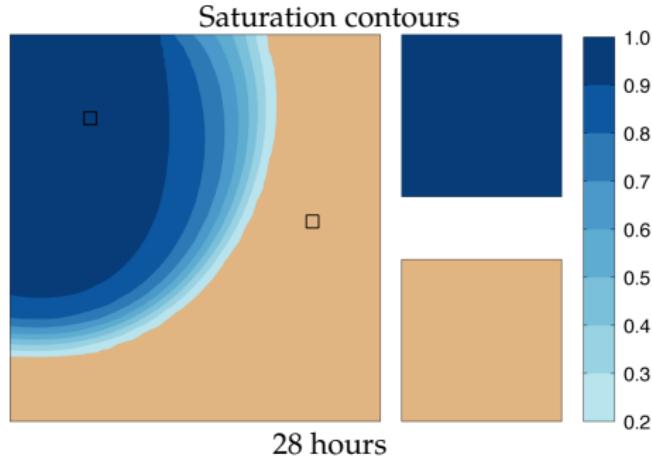
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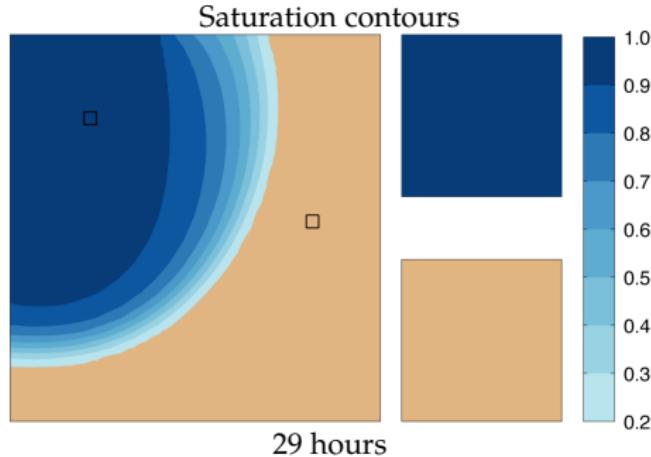
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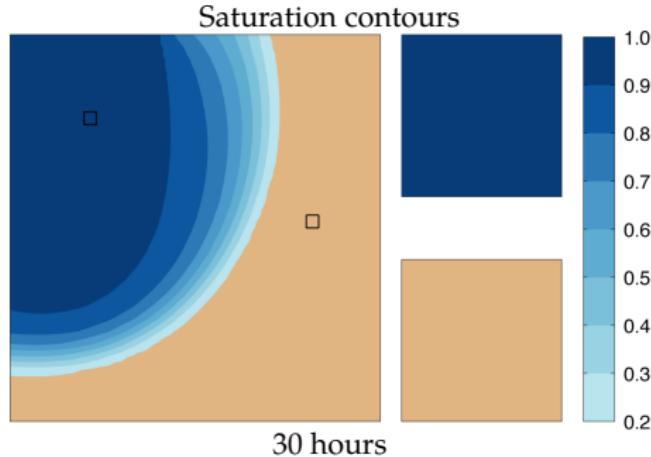
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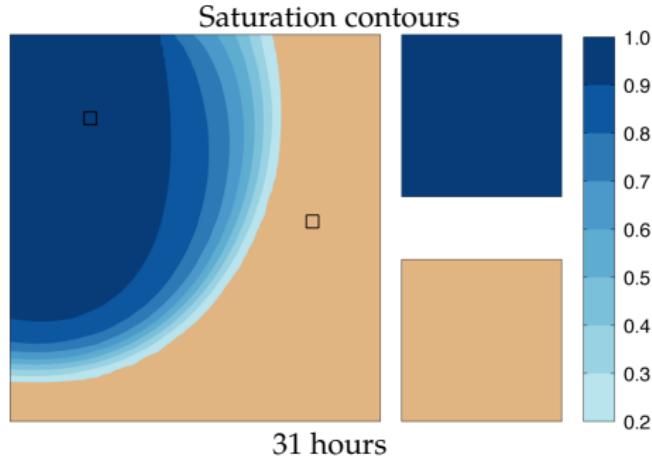
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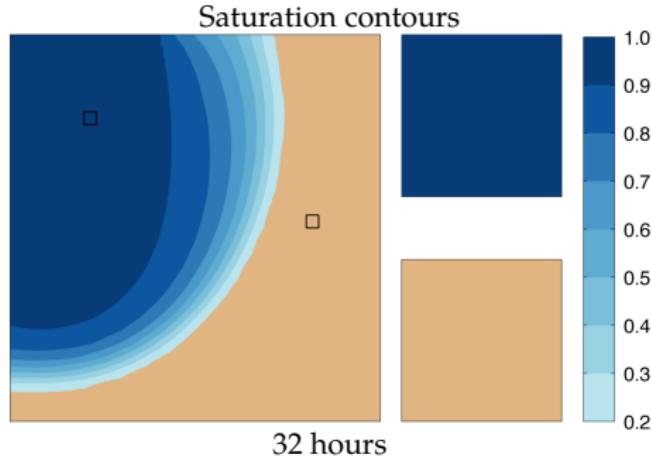
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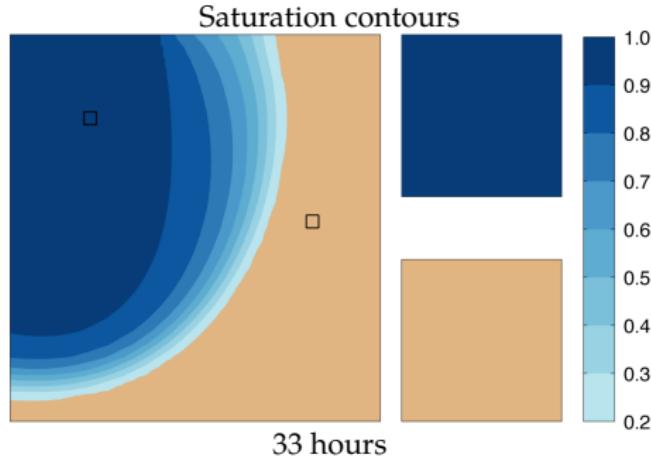
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



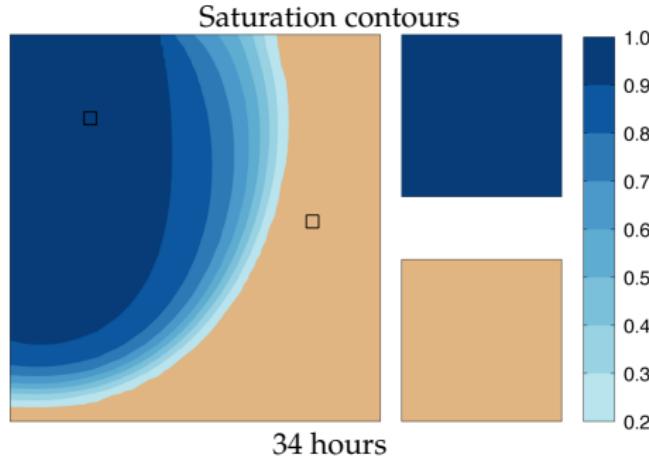
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



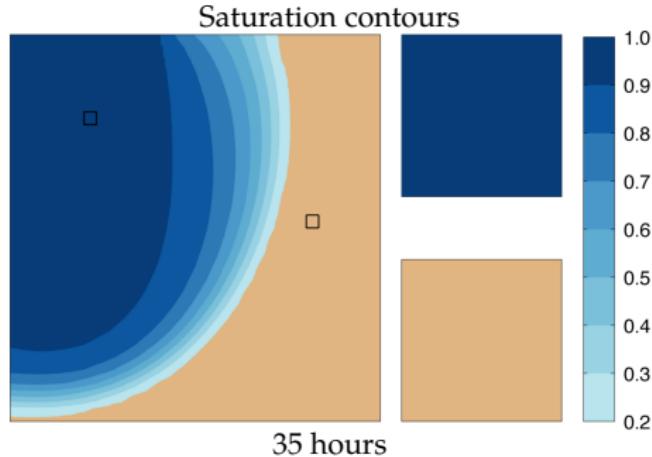
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



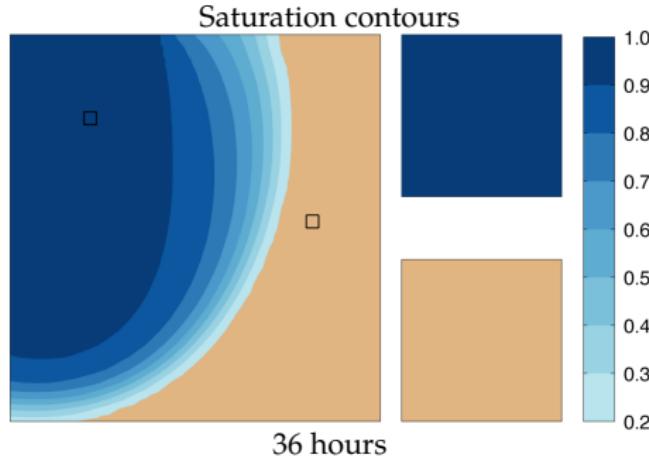
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



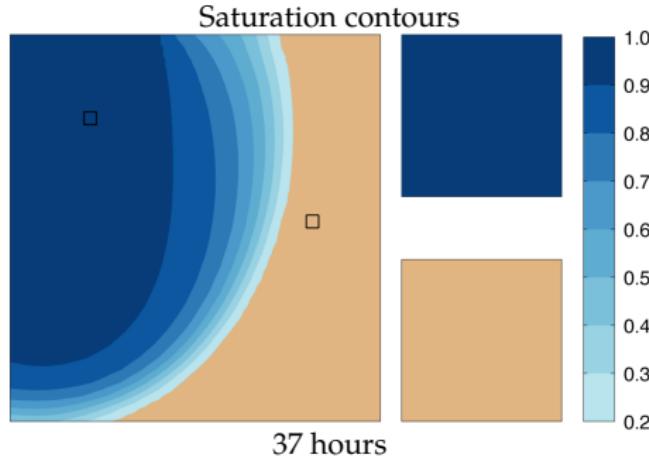
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



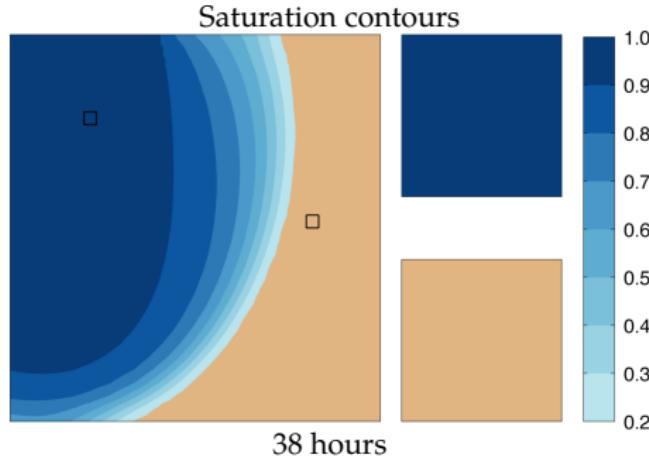
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



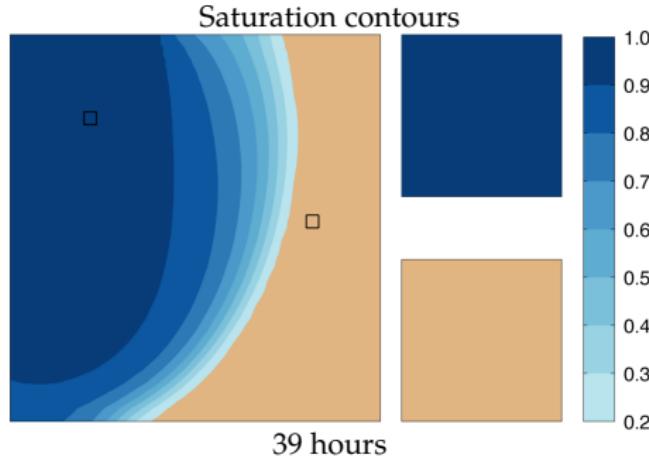
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



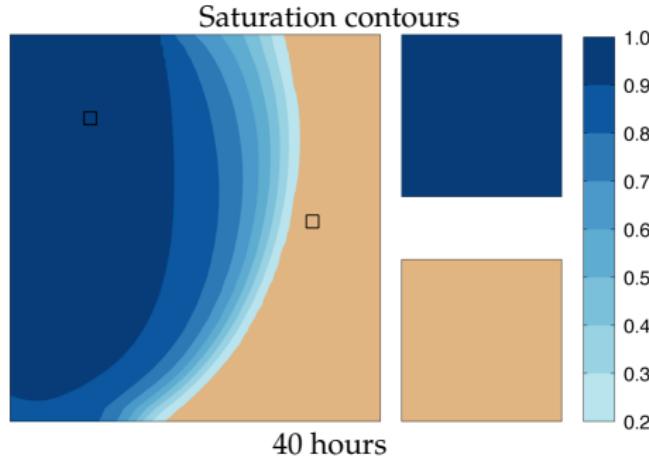
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



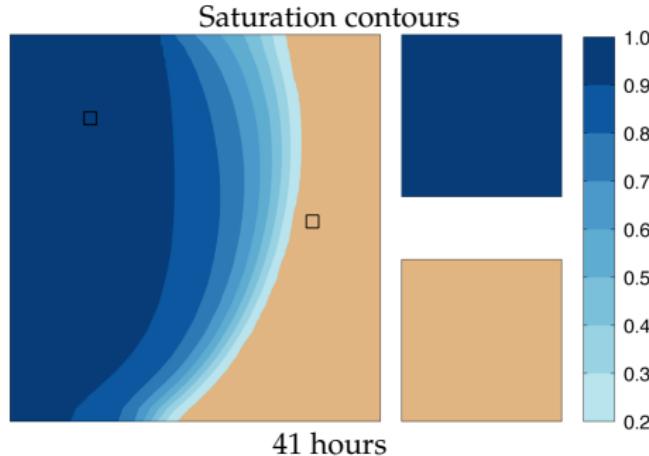
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



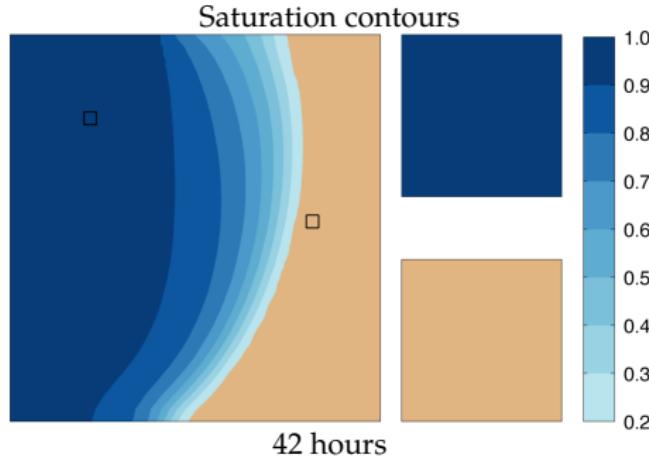
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



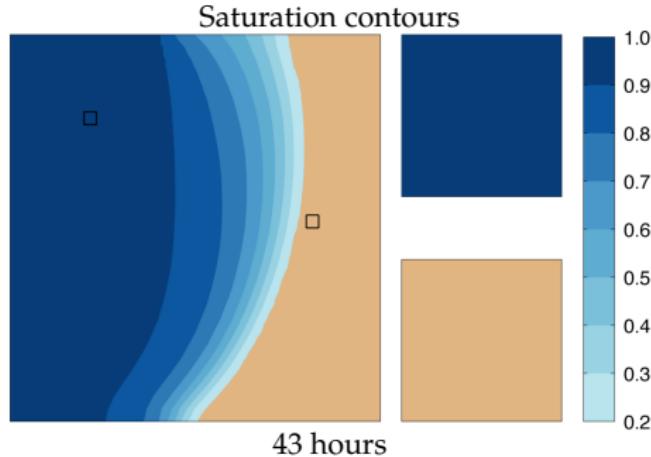
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



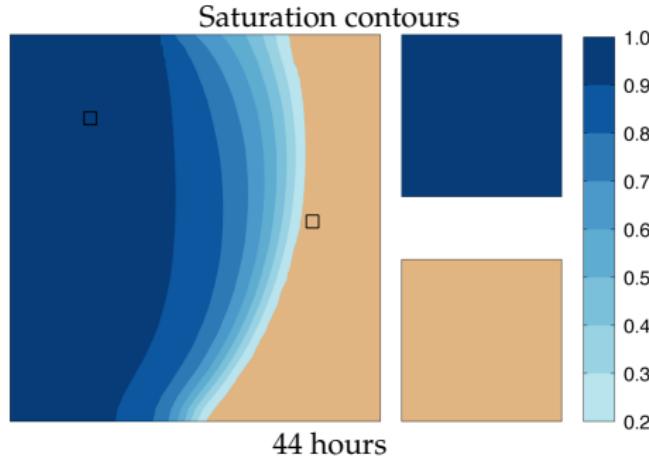
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



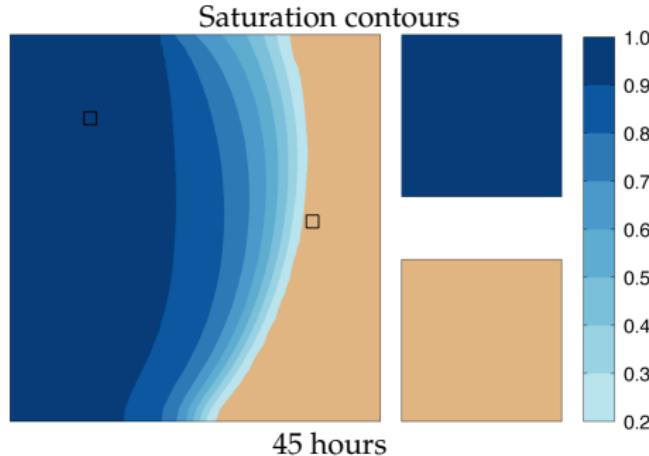
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



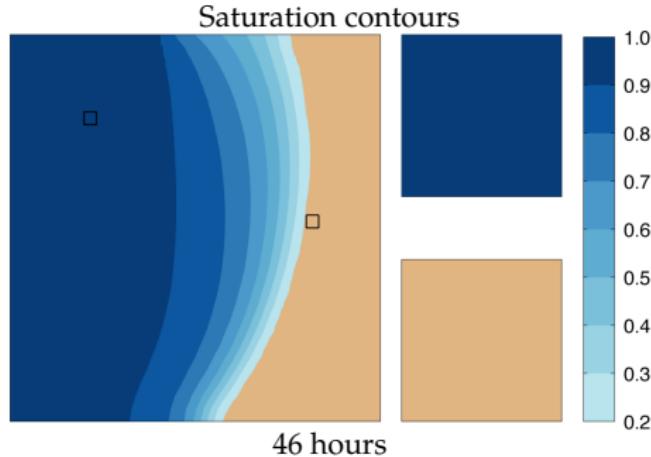
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



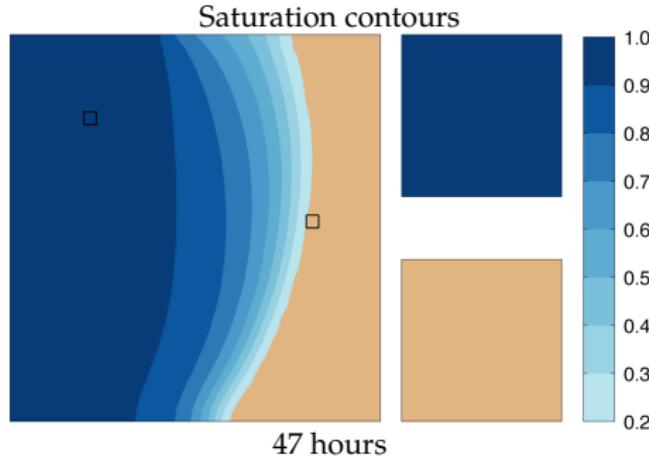
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



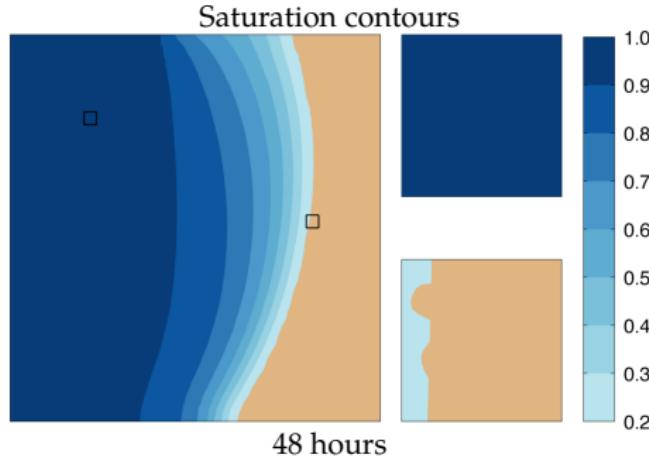
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



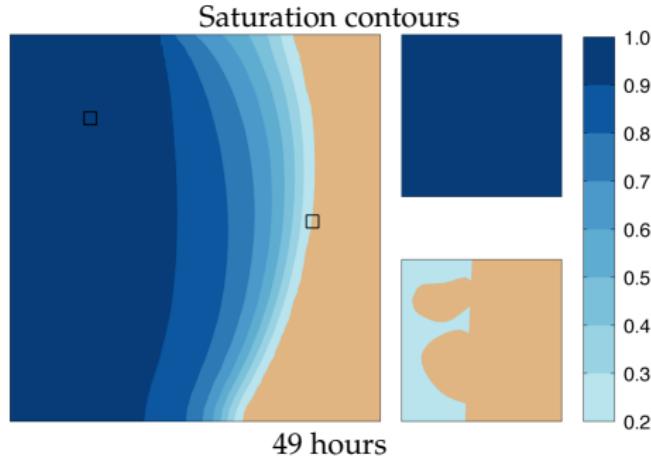
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



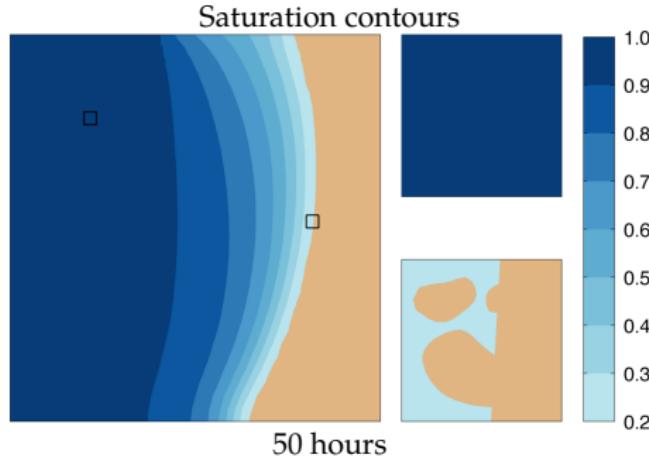
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



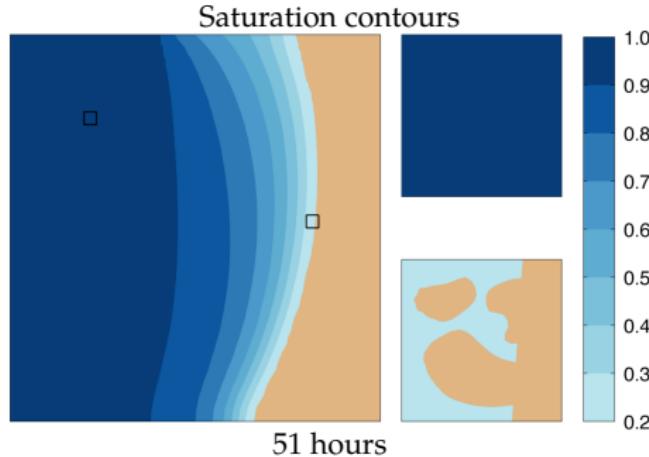
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



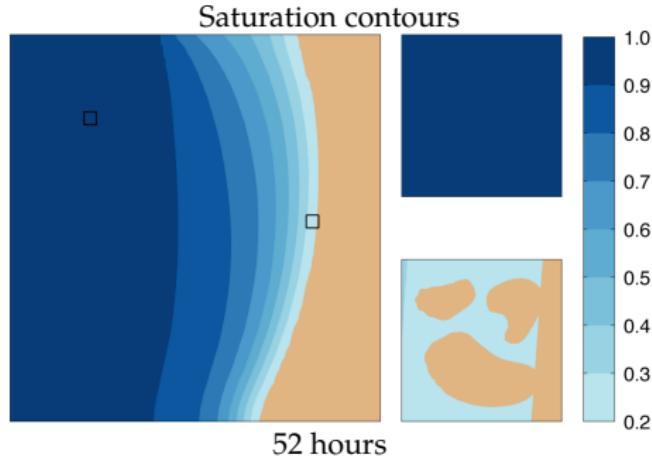
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



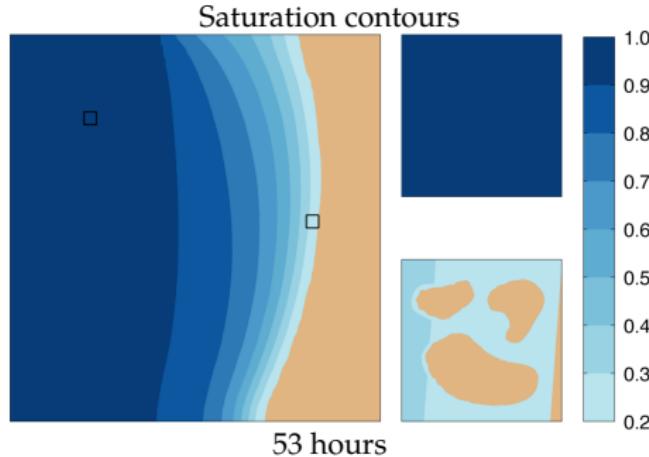
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



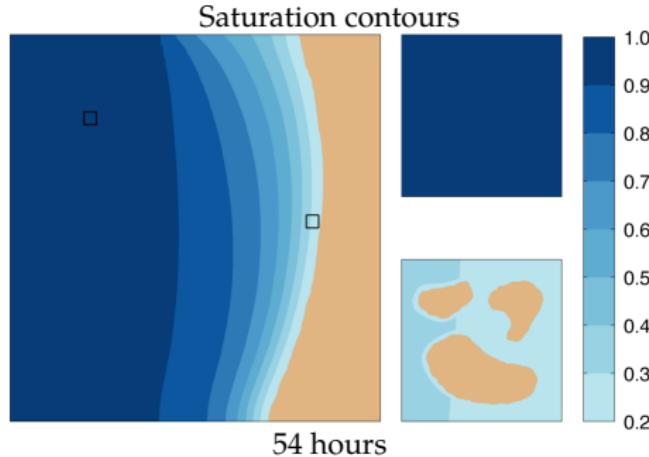
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



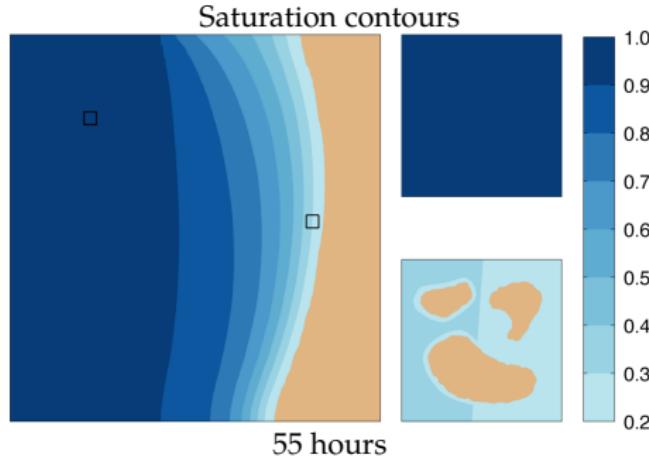
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



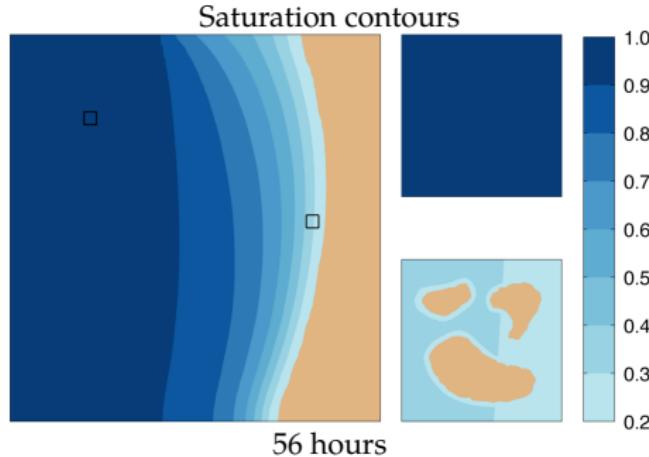
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
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Simulation: Unsaturated water flow



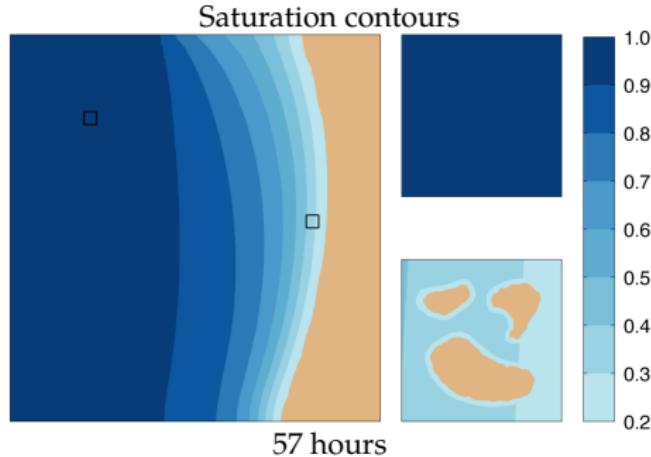
	Serial	1 core	2 cores	4 cores	8 cores
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Simulation: Unsaturated water flow



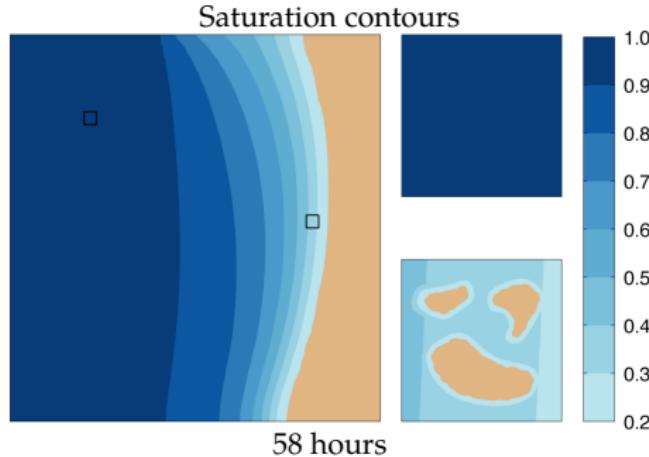
	Serial	1 core	2 cores	4 cores	8 cores
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Simulation: Unsaturated water flow



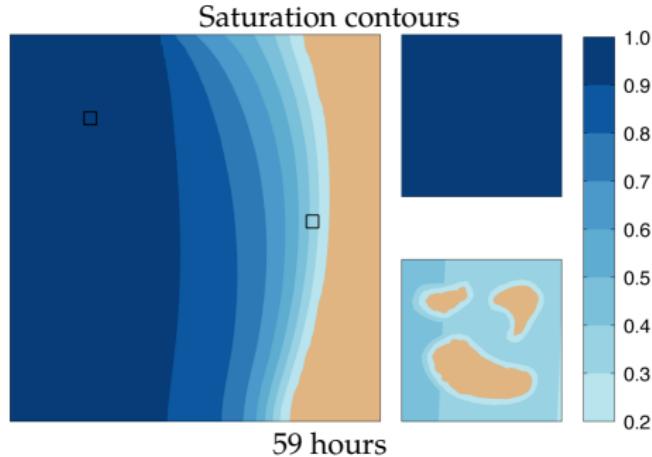
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



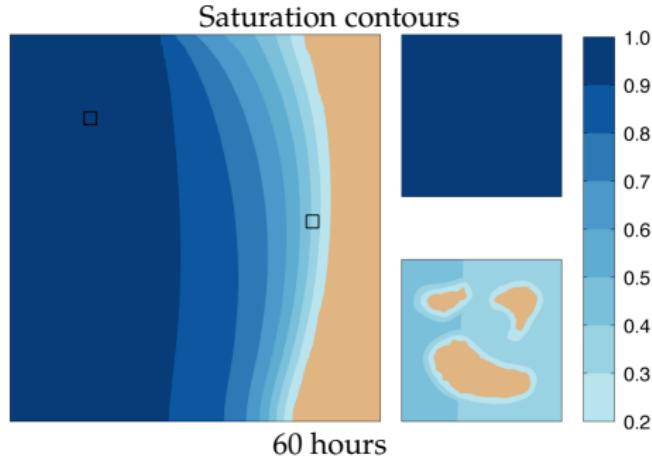
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



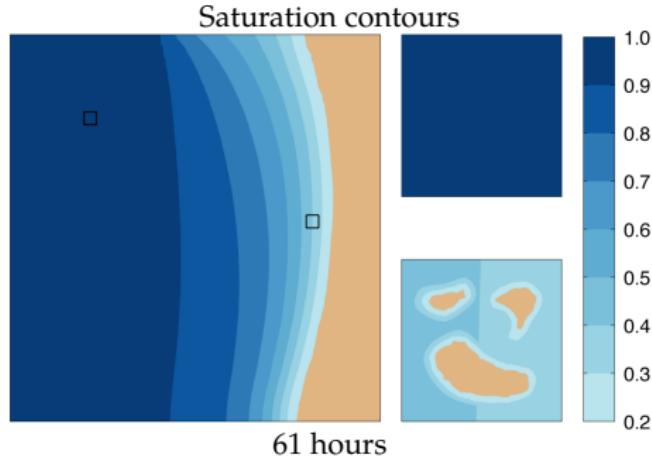
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



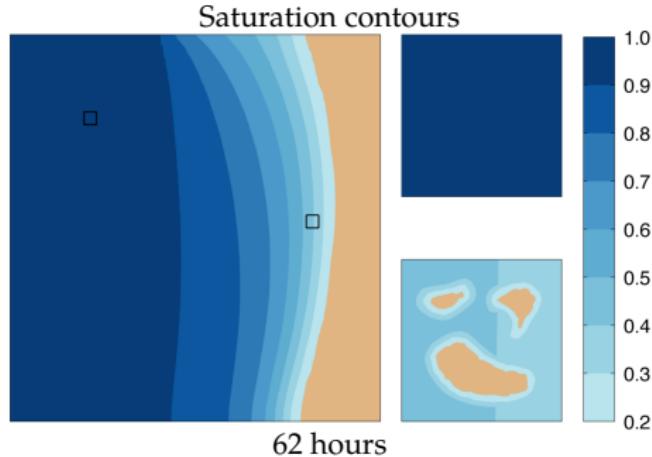
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



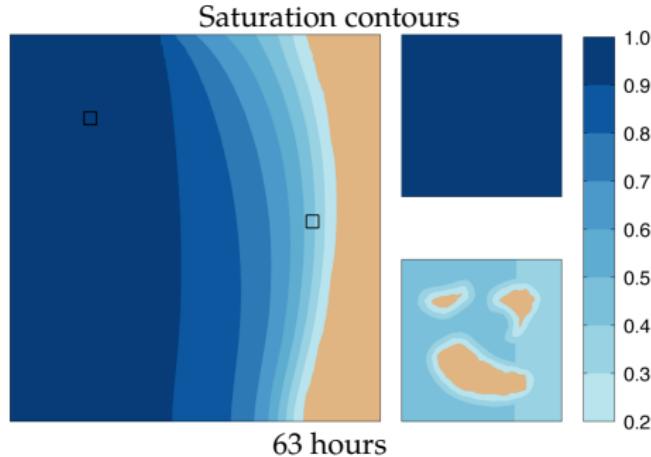
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Simulation: Unsaturated water flow



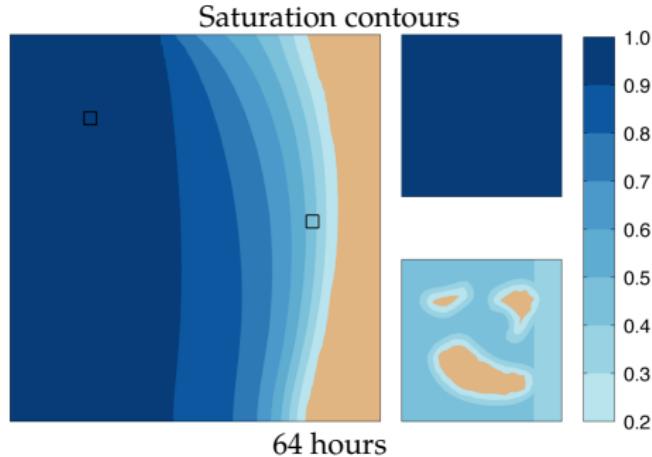
	Serial	1 core	2 cores	4 cores	8 cores
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



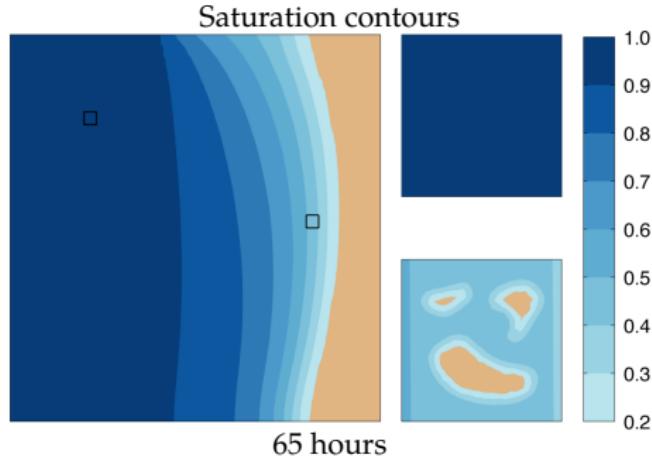
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
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Simulation: Unsaturated water flow



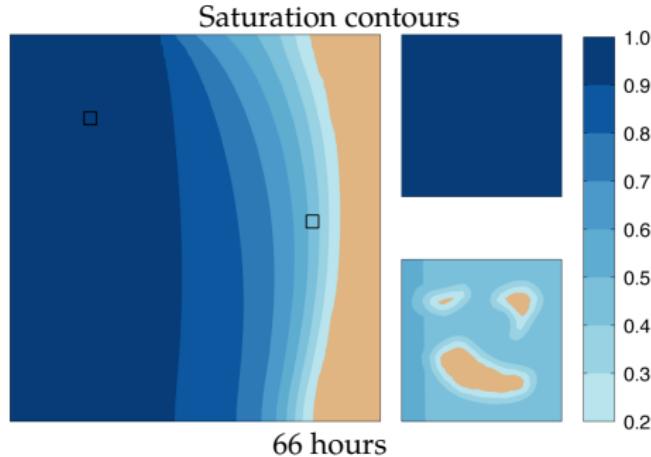
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Runtime (min)	179	182	94	51	31
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Simulation: Unsaturated water flow



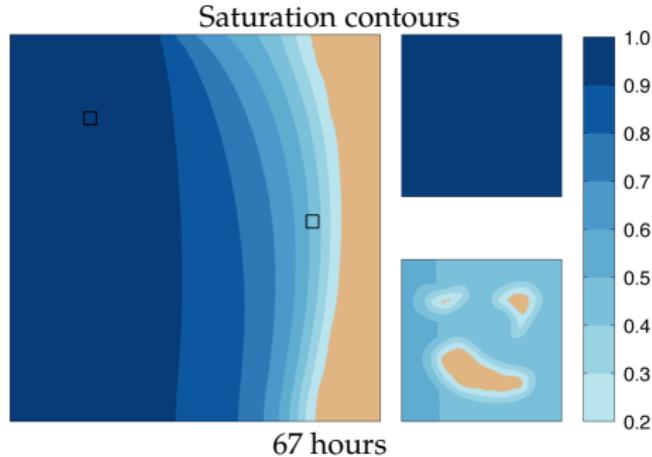
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



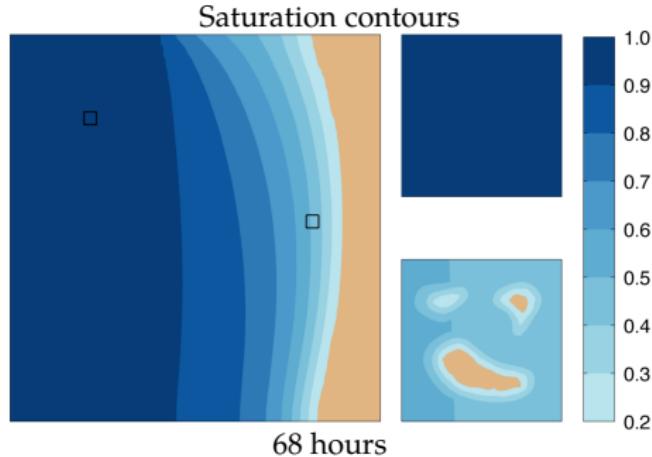
	Serial	1 core	2 cores	4 cores	8 cores
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Simulation: Unsaturated water flow



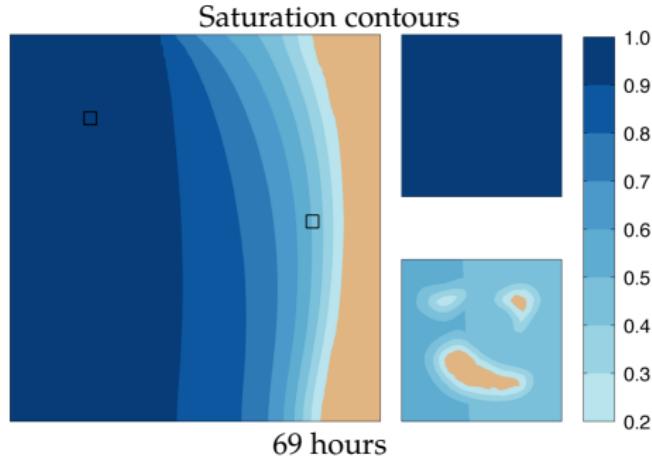
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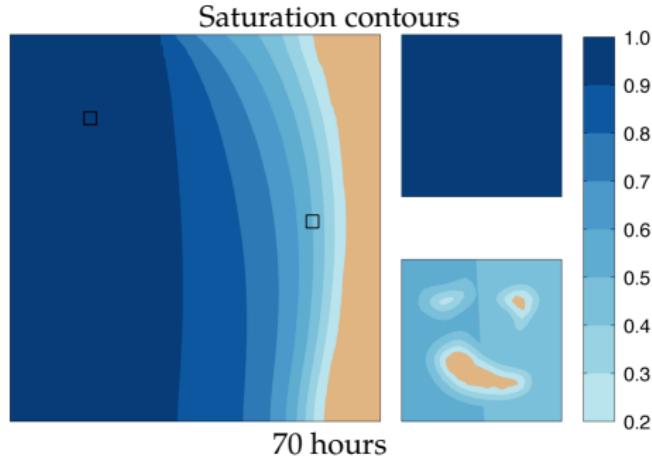
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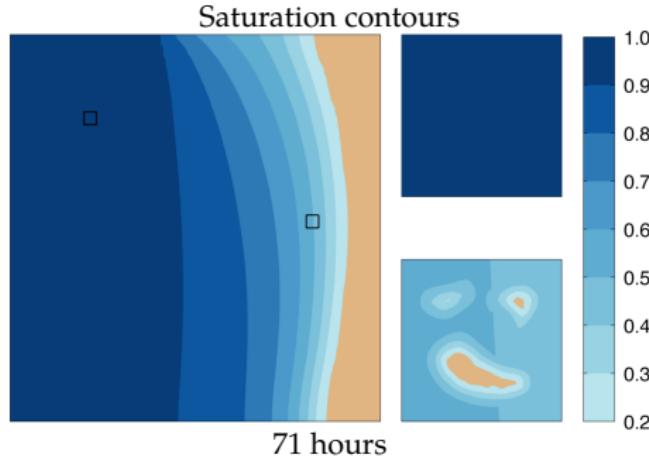
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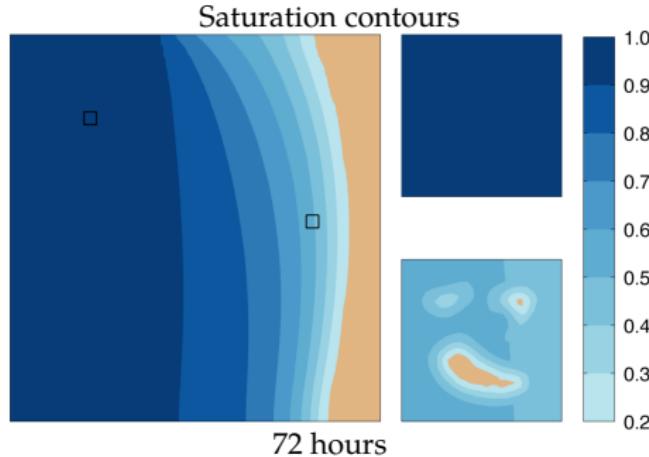
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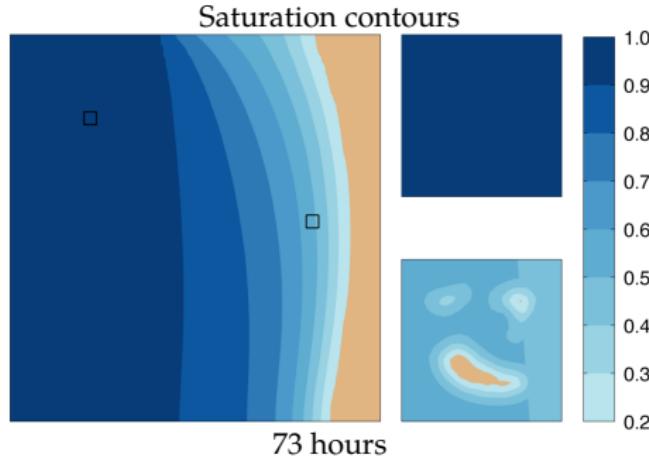
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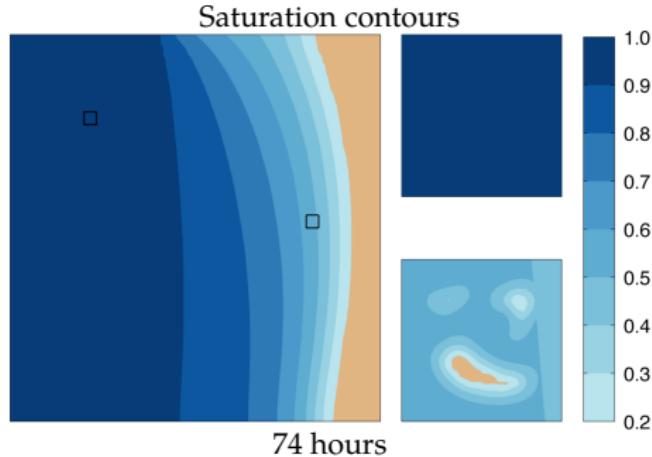
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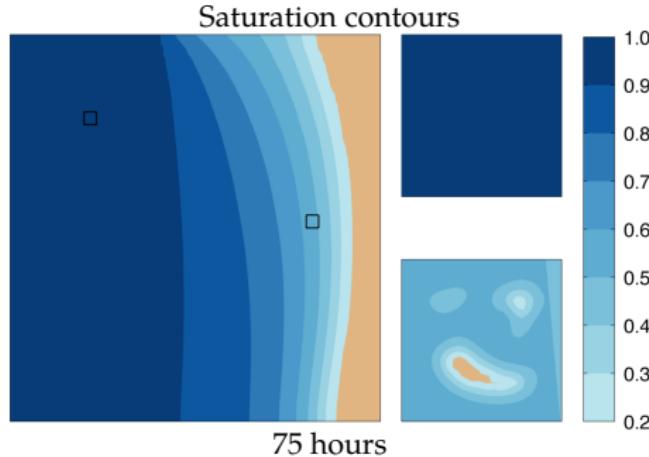
	Serial	1 core	2 cores	4 cores	8 cores
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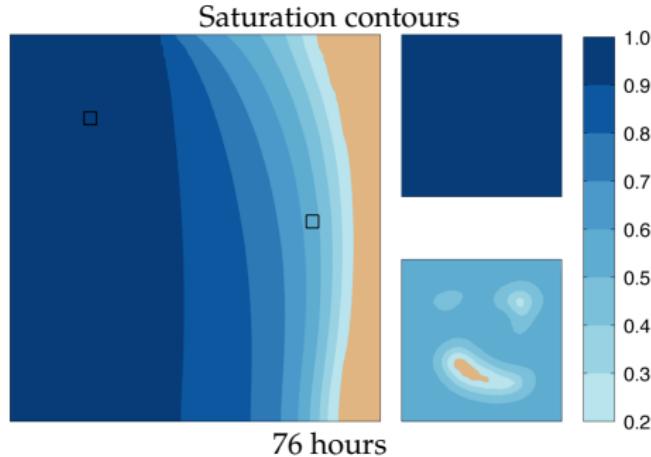
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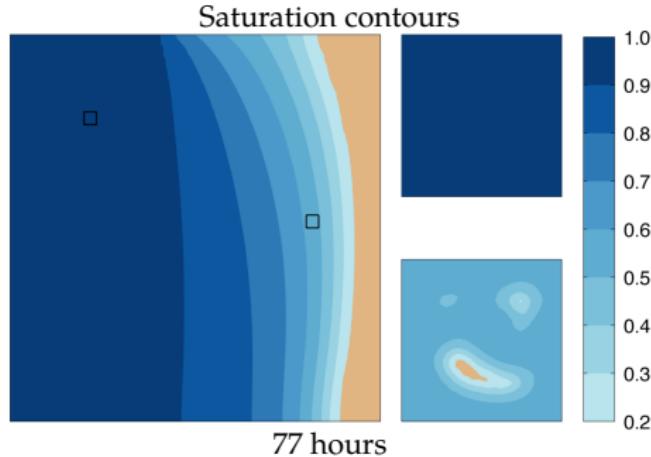
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Simulation: Unsaturated water flow



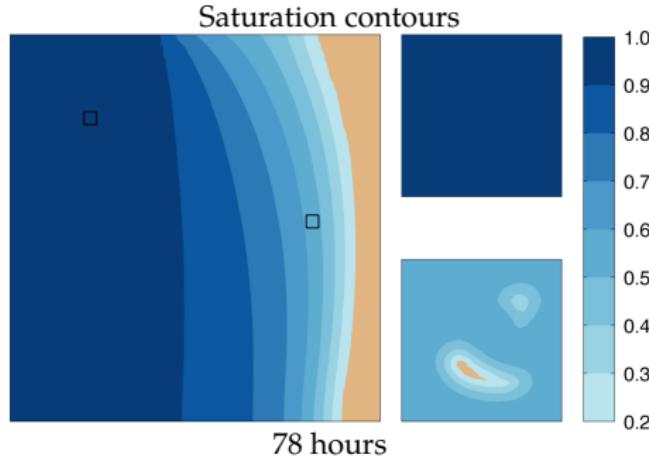
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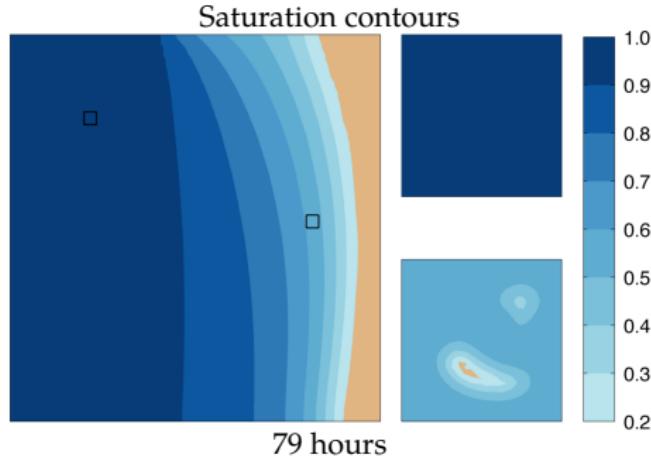
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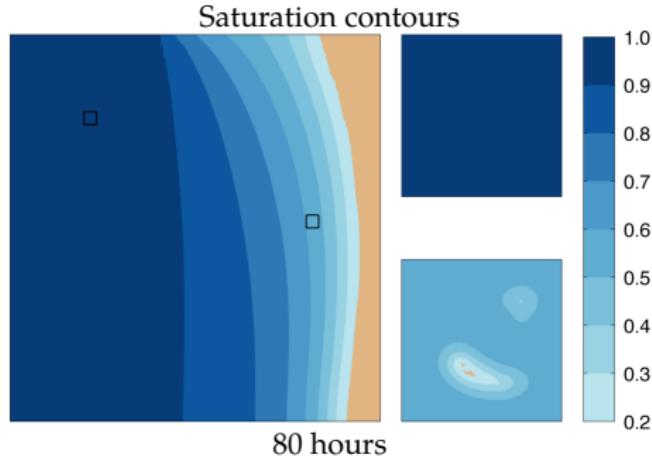
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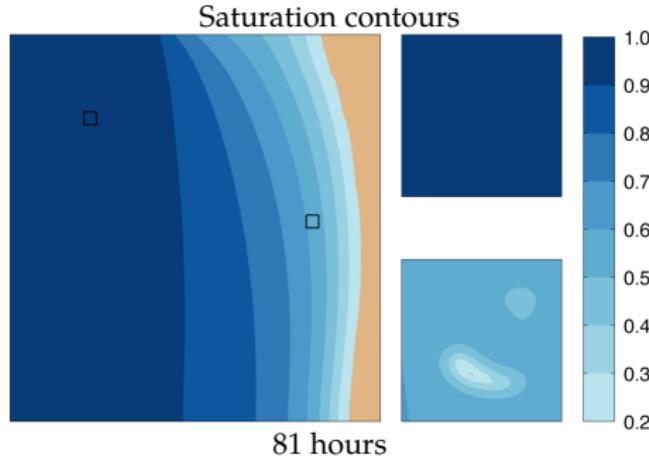
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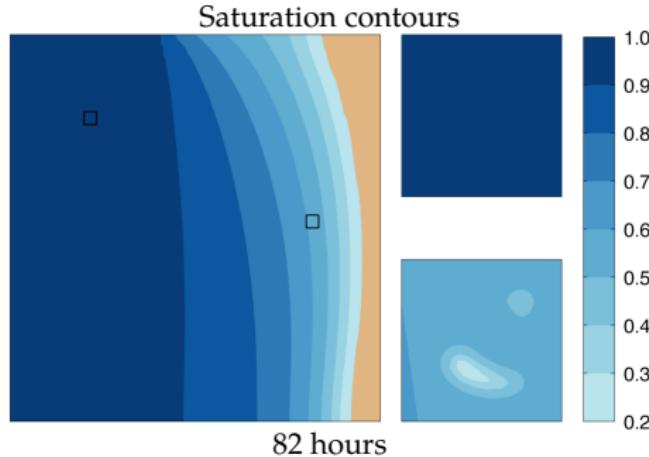
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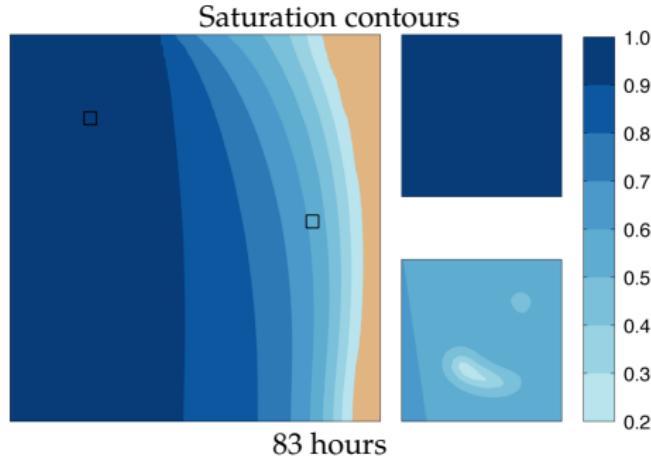
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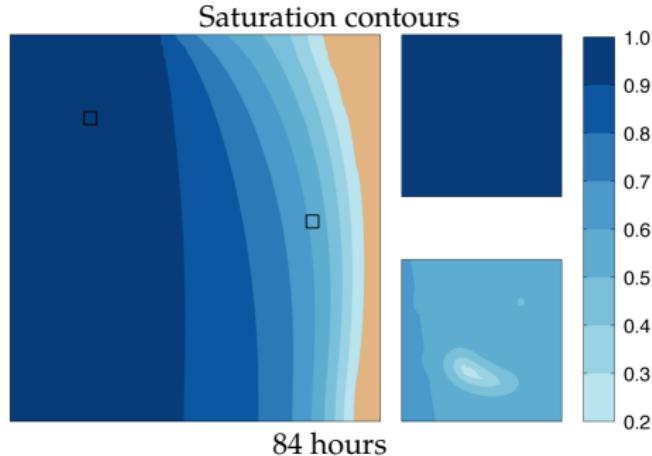
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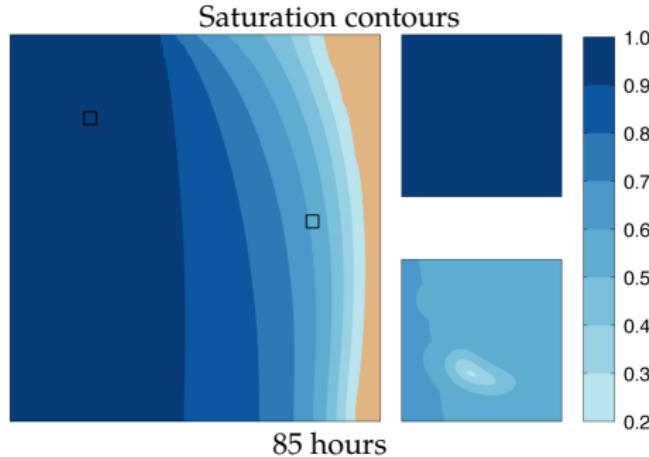
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Simulation: Unsaturated water flow



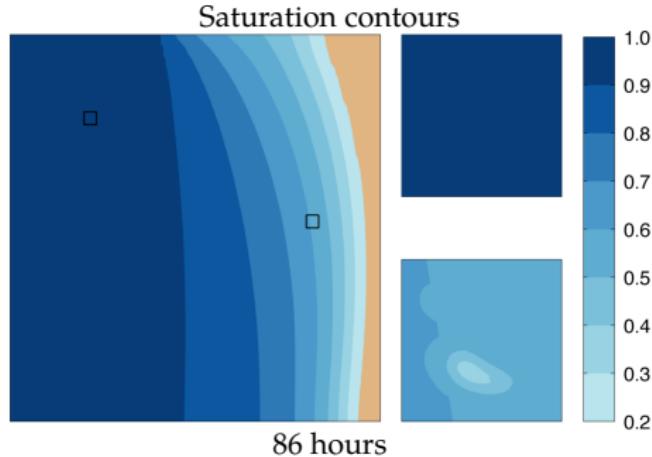
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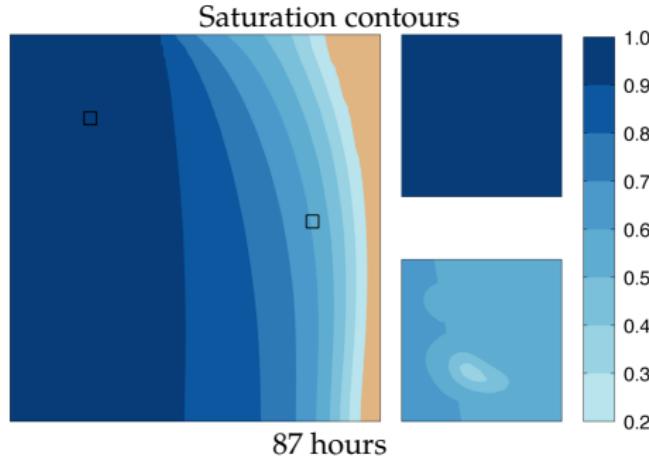
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Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



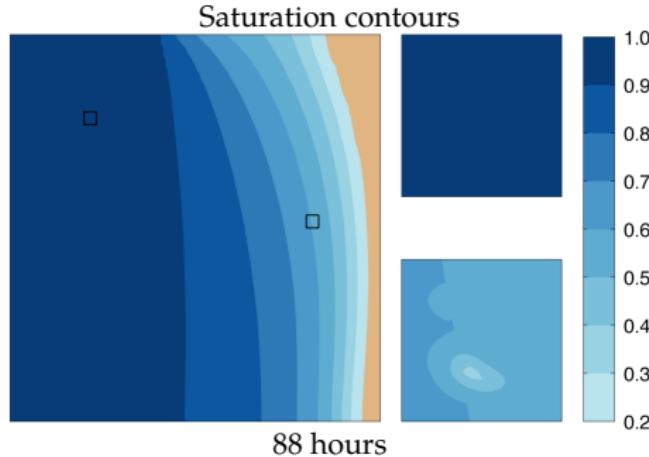
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



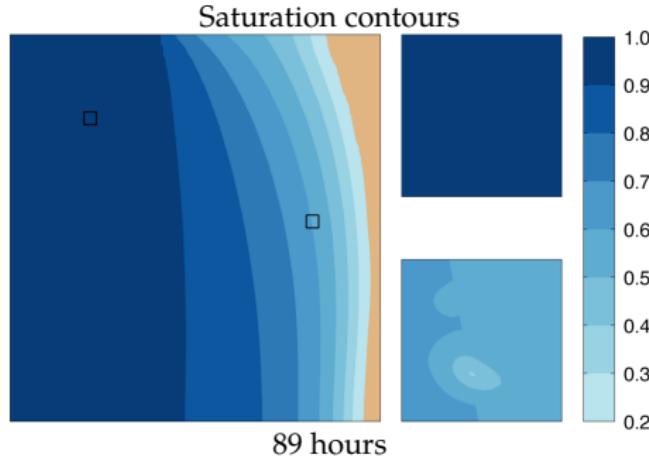
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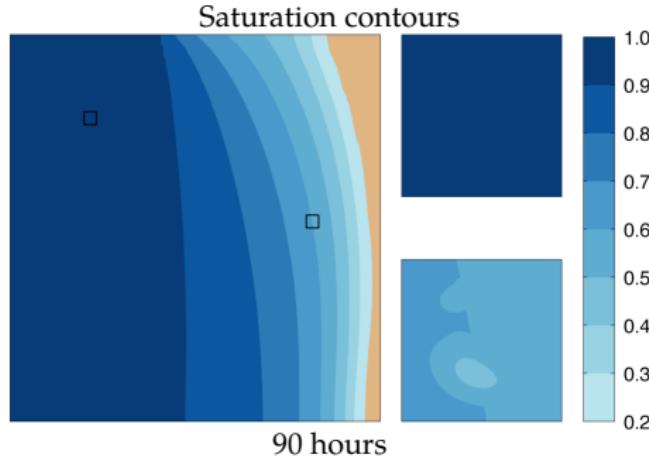
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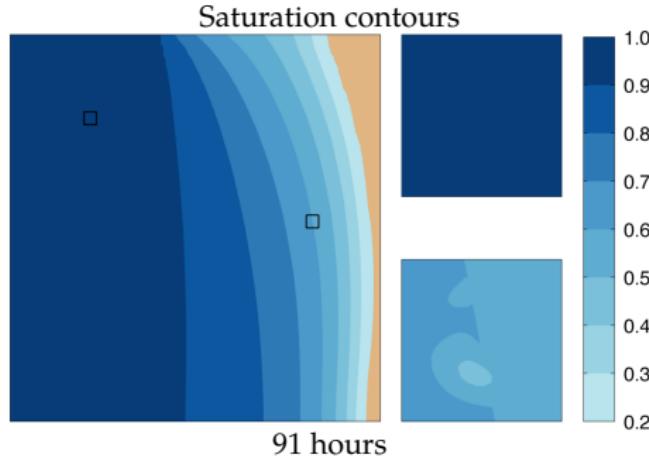
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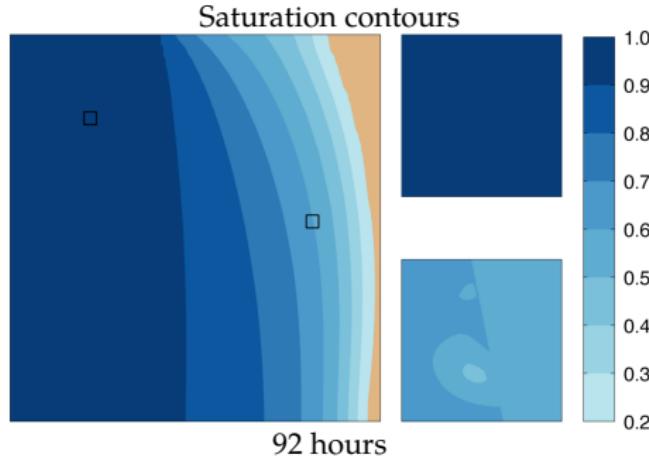
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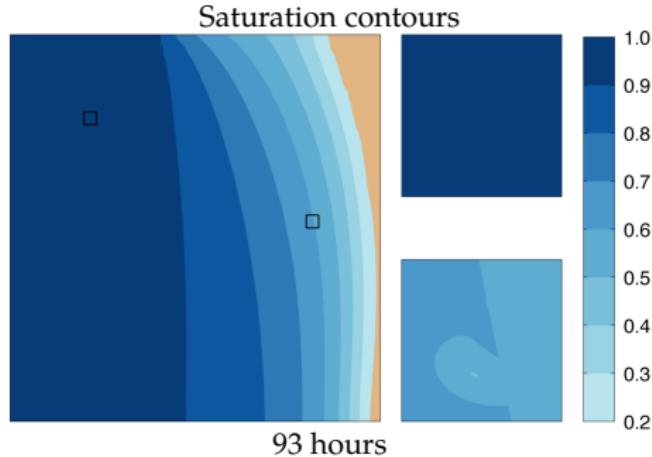
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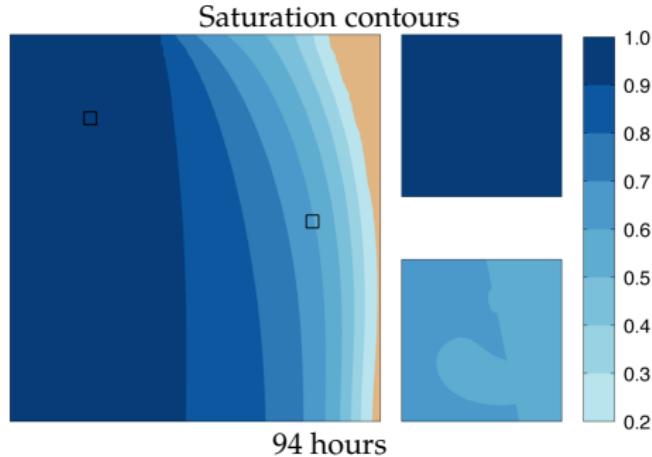
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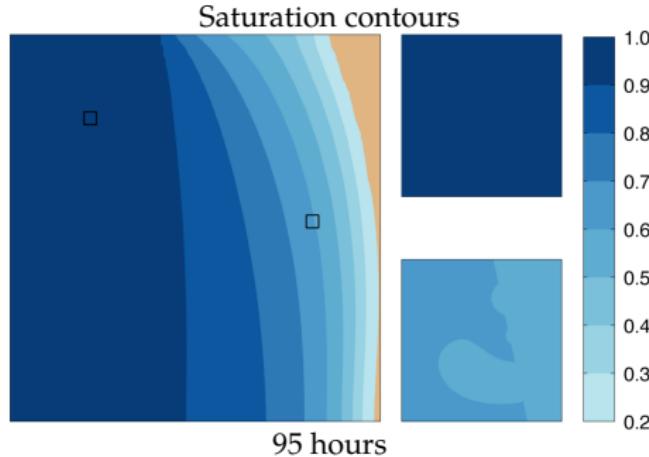
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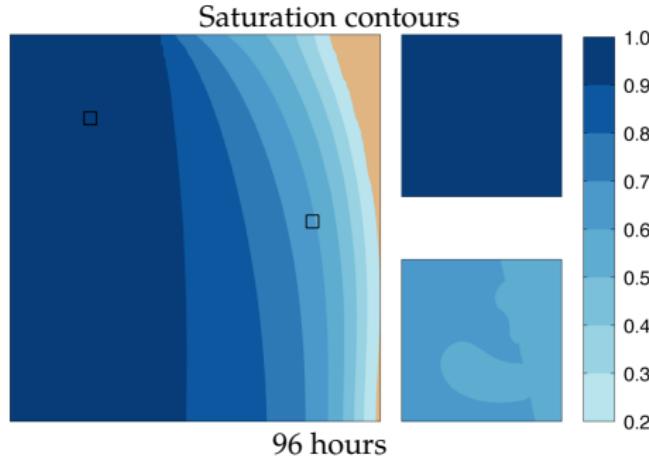
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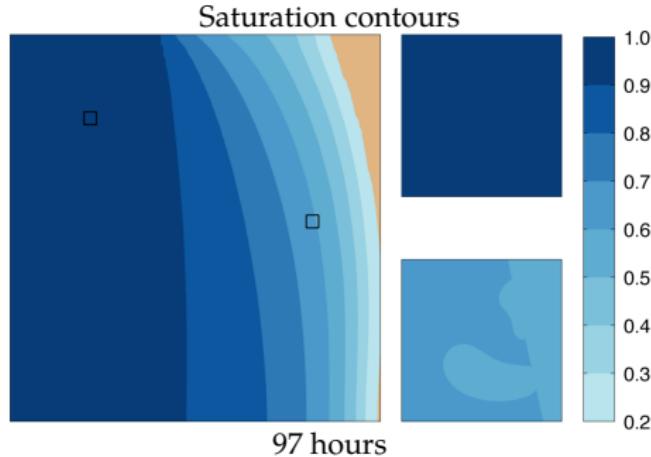
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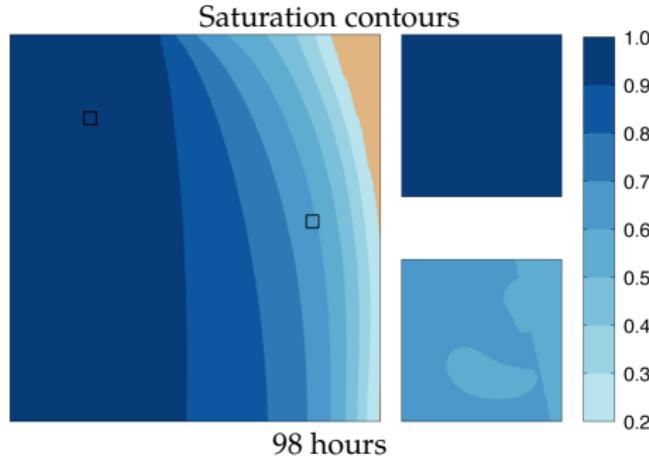
	Serial	1 core	2 cores	4 cores	8 cores
Runtime (min)	179	182	94	51	31
Speedup	1.00	0.98	1.90	3.50	5.84

Simulation: Unsaturated water flow



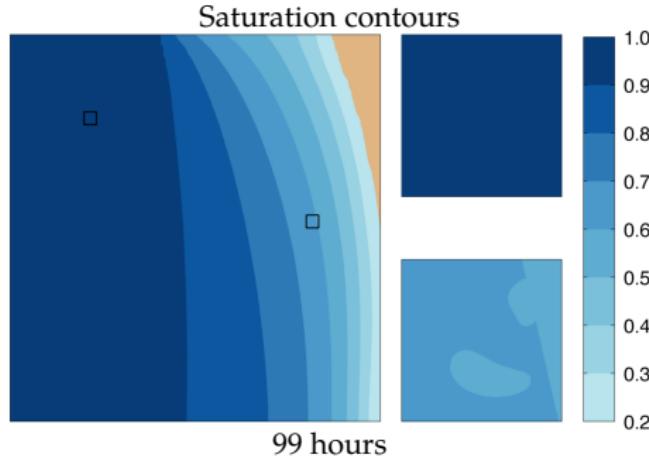
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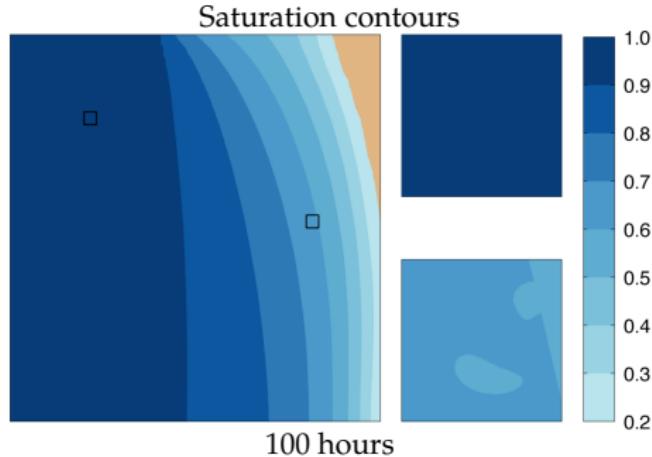
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Summary and Conclusions

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- ✓ Ability to capture fine-scale detail in the full heterogeneous problem
- ✓ Produces good qualitative agreement with fine-scale model
- ✓ Significant reduction in simulation time (compared with fine-scale model)
- ✓ Numerically feasible for problems with very small-scale heterogeneities
- ✗ Restricted to heterogeneous domains comprised of two sub-domains where one is connected and the other forms disconnected/isolated inclusions

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Questions?

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